

FOW Subgroup Workshop

TIC Glasgow, 22nd August



Programme

12.30 - Introduction – Subgroup Co-Chairs

12.40 - Industry and project updates – floating wind projects in the pipeline

- 1) **Richard Wakefield – Flotation Energy**
- 2) **David Timmington – FWO**
- 3) **Takashi Harada – Toda Corporation**

13.10 – Mooring Systems Session 1

- 1) **Alan Duncan – Intermoor**
- 2) **Fredrik von der Fehr – DOF Subsea**
- 3) **Bill Shaw – Bauer Renewables**

13.55 – Networking coffee break

14.20 – Mooring Systems Session 2

- 1) **Ferdinando Samona – Maersk**
- 2) **Stuart Kilbourn - Fugro**
- 3) **Elsa Ramirez – Leask Marine**
- 4) **Stein Are Anderson – Bridon Bekaert**

15.20 – Co-chairs summation and next steps

15.30 – End of workshop

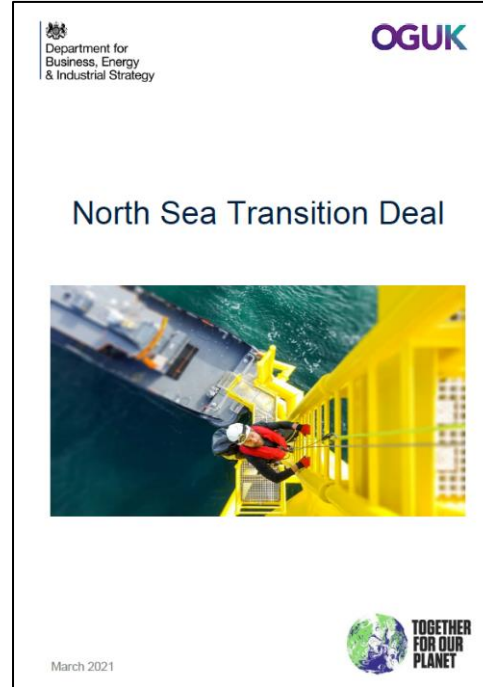
Green Volt Offshore Wind

23rd August 2022

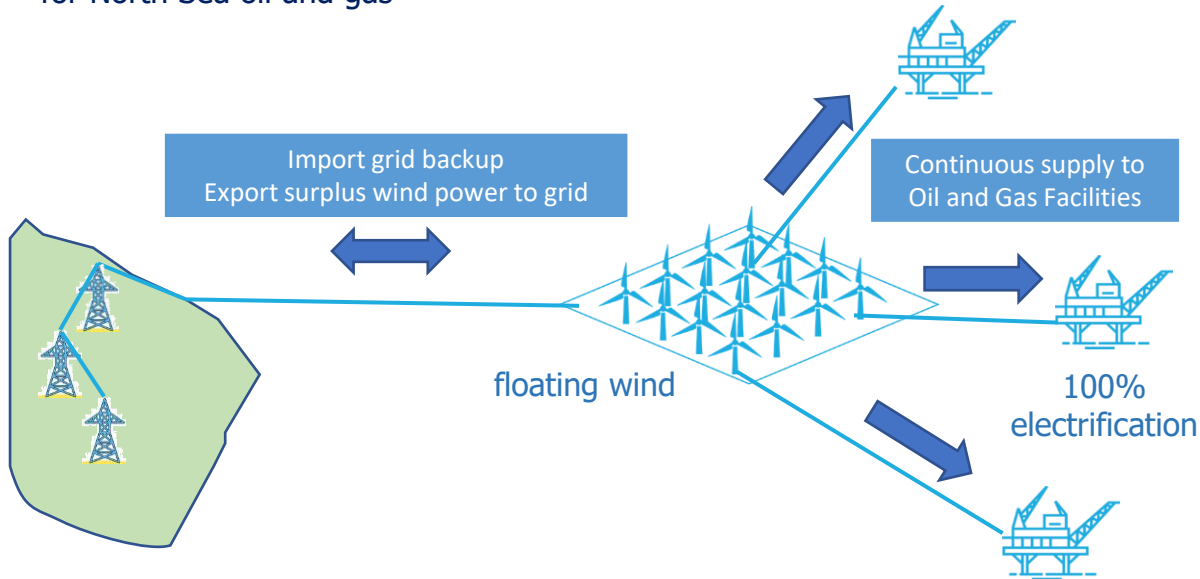
Deep Wind Update



- UK oil and gas assets part of the Energy Transition
- North Sea Transition Deal goal
- 50% emission reduction by 2030
- Net Zero basin by 2050

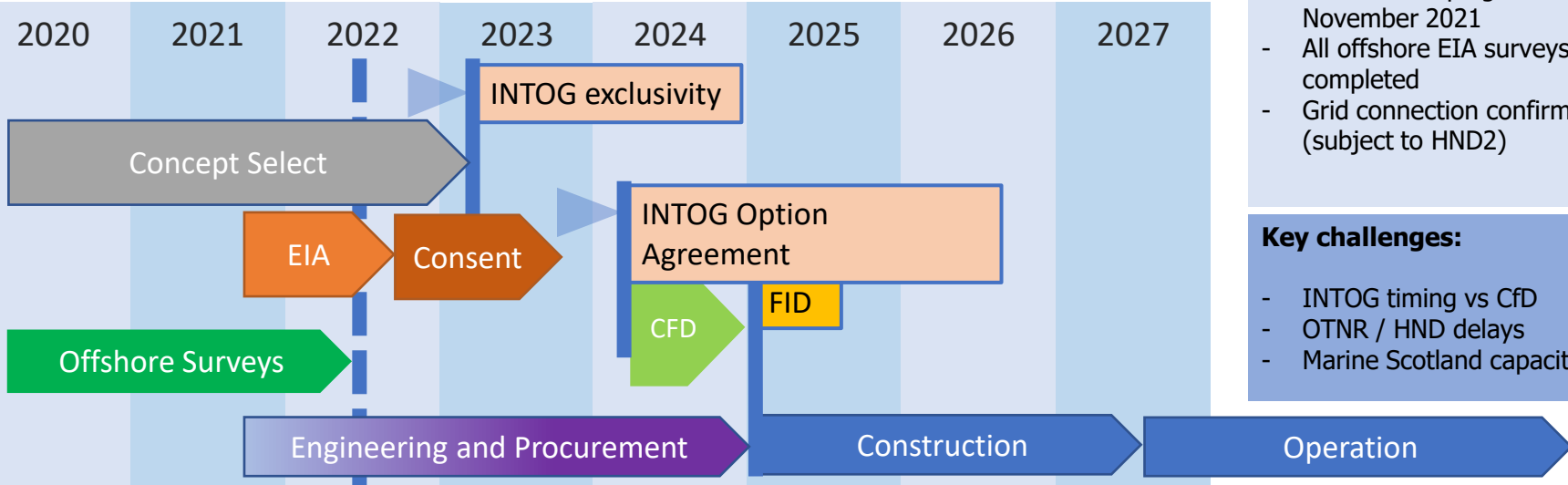


- Grid connected floating offshore wind farm to power UKCS O&G
- 100% retirement of onboard power generation
- Leverage offshore demand and CFD to provide affordable, renewable electricity for North Sea oil and gas



- ✓ 100% electrification
- ✓ Rapid deployment
- ✓ Maximum decarbonisation
- ✓ Grid reliability
- ✓ Fully eliminate GTG maintenance costs
- ✓ No late life gas buy back
- ✓ Optimal CapEx
- ✓ UK offshore wind growth targets

Green Volt Project – Project Overview



Key milestones:

- Offshore Scoping submitted November 2021
- All offshore EIA surveys completed
- Grid connection confirmed (subject to HND2)

Key challenges:

- INTOG timing vs CfD
- OTNR / HND delays
- Marine Scotland capacity

Open Discussion





Goto Pilot Farm

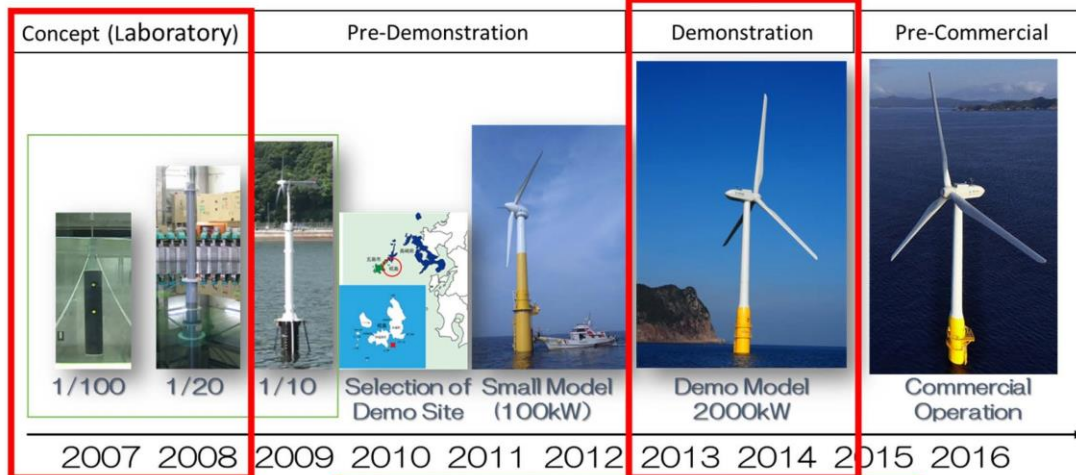
OCEAN RENEWABLE ENERGY DIV.
TODA CORPORATION
TAKASHI HARADA



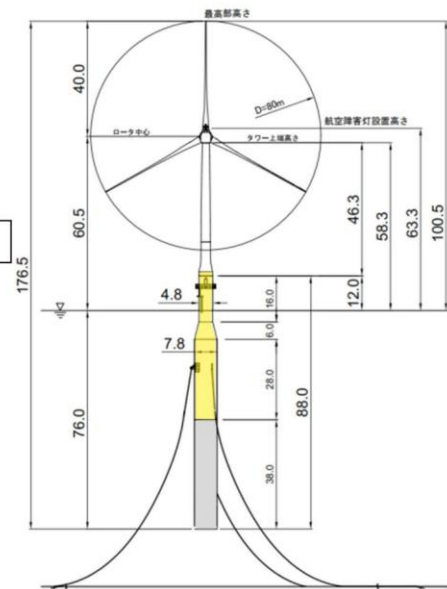
Prof. Tomoaki Utsunomiya



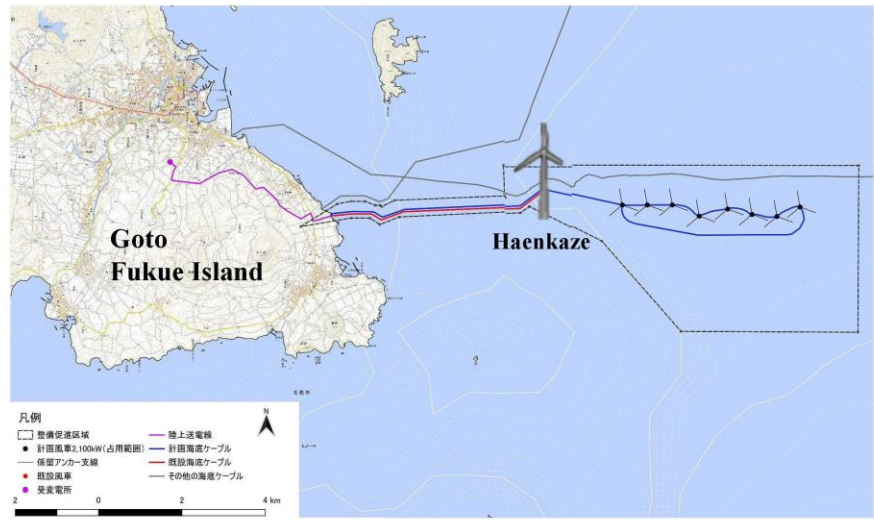
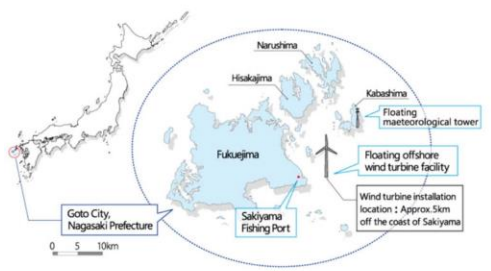
Dr. Iku Sato



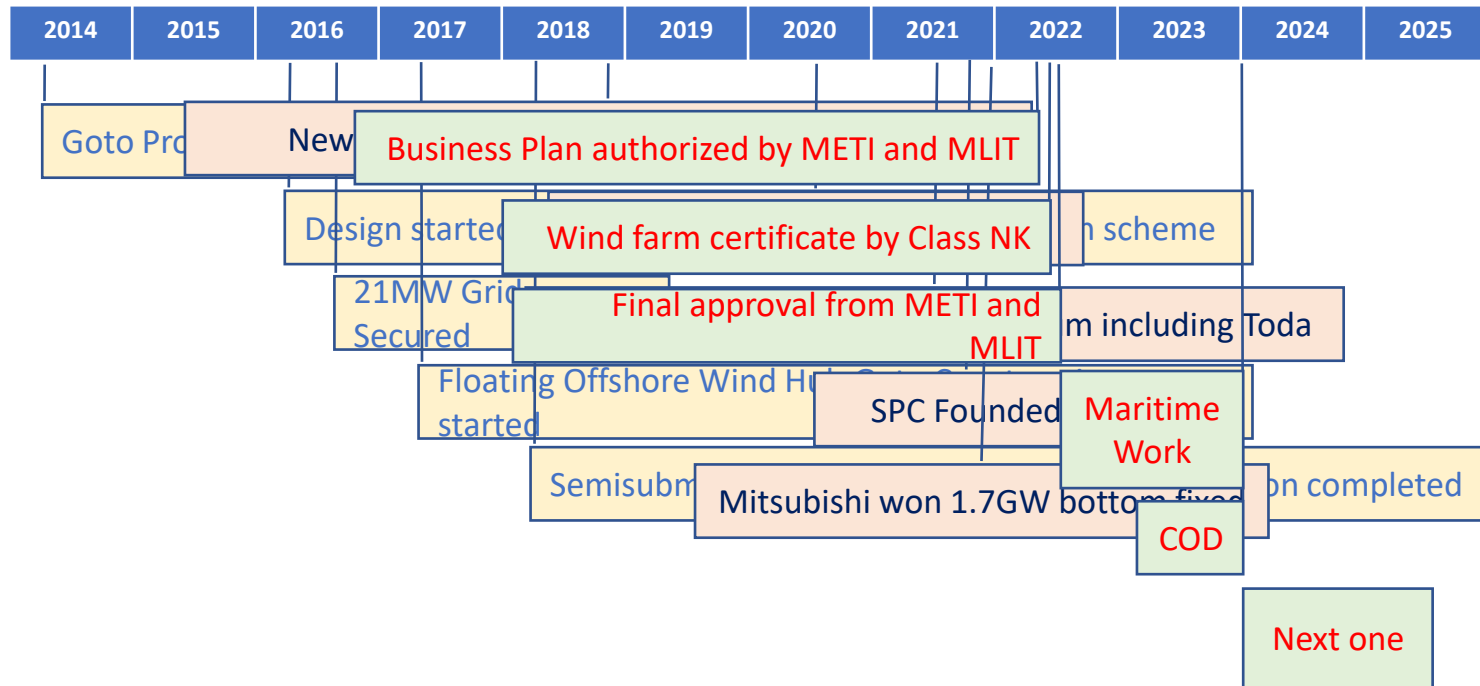
Project by the Ministry of Environment (from 2010 to 2015)



Goto Pilot Farm



Goto Pilot Farm



Manufacturing Process

Anywhere

Utilizing local ordinary port

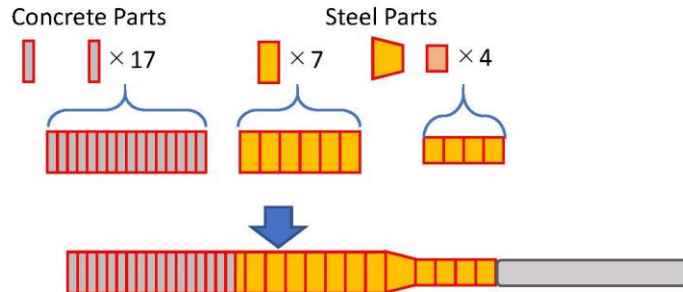
Production locally

Horizontal process

Anyone

Simple manufacturing process

Assembly same size rings



Floating Offshore Wind Hub Goto

Installation Process

Cost effective process
No JUV nor Heavy crane vessel

Float Raiser
< 5m draft
Semi-submersible
Sink – Drag – Raise-up



“Anyone Anywhere AS required”

- Anyone
 - Simple design
 - Simple manufacturing process
- Anywhere
 - Less than ideal condition
- As required
 - Any turbine
 - Adapting wide range of water conditions

INTERMOOR

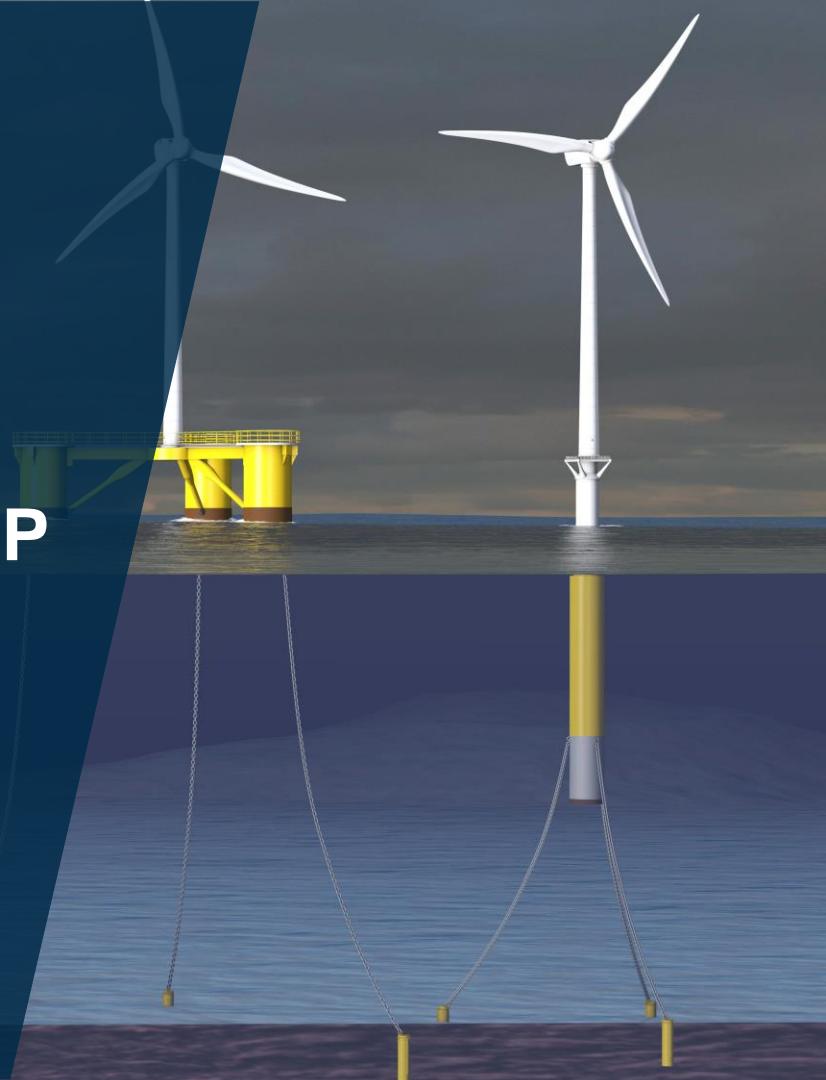
Mooring specialist – providing mooring system design, supply storage and management of mooring equipment and marine services for installation, maintenance and decommissioning

DEEPWIND FOW SUBGROUP EVENT 23RD AUGUST

ACTEON



MOORINGS AND ANCHORS



AGENDA:

- Planning – Scheduling
- Supply Chain & Design Constraints
- Product standardization
- R&D – future planning



Planning ahead

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MOORINGS AND ANCHORS

When timings are known for mooring equipment and production scheduling can be considered.....

Anything is possible.

Currently, one of the largest mooring chain carousel manufacturing plants was designed, built and commissioned in less than 12 months.

This carousel can produce chain links up to 230mm in diameter.



Planning and capacity

Currently InterMoor have the capacity to supply a total of 300,000tons of chain (annually).

However, this could only be considered if suitable forward planning and production scheduling can be looked at – well in advance.

To allow 300,000t of chain to be supplied annually, the current factories would need to increase their output to at least 500,000t to provide for the legacy O&G, shipping, fishing industries.



Capacity

300,000t of chain in terms of size/length:

- 84mm studless chain (600/850t MBL) = 2,150,000m = 1336 miles
- 120mm studless chain (1100/1600t MBL) = 1,037,000m = 644 miles
- 180mm studless chain (1500/2400t MBL) = 461,000m = 287 miles



Product Standardization

ACTEON



MOORINGS AND ANCHORS

To enable the smooth transition to floating wind mooring systems, the lessons learned from O&G must be taken on board.

Petrobras had at least 4 different chain sizes on the earliest of their mooring systems offshore Brazil.

Today? A high percentage of systems offshore Brazil are 120mm studless chains manufactured in a dedicated factory in-country.

Thus, production and scheduling can be controlled in a logical manner.



Product Complexity and Risk

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MOORINGS AND ANCHORS

Product complexity, size and manufacturing lead-time MUST be considered for FOWT.

Complex systems with non-track-record items can only be grouped as “potential threats” offshore.

Theses “threats” could mean catastrophic failure of windfarms which could mean loss of required onshore power supply.

Planning of the mooring system is critical not just in terms of manufacturing lead-time but also in terms of installation and maintenance requirements in the future.

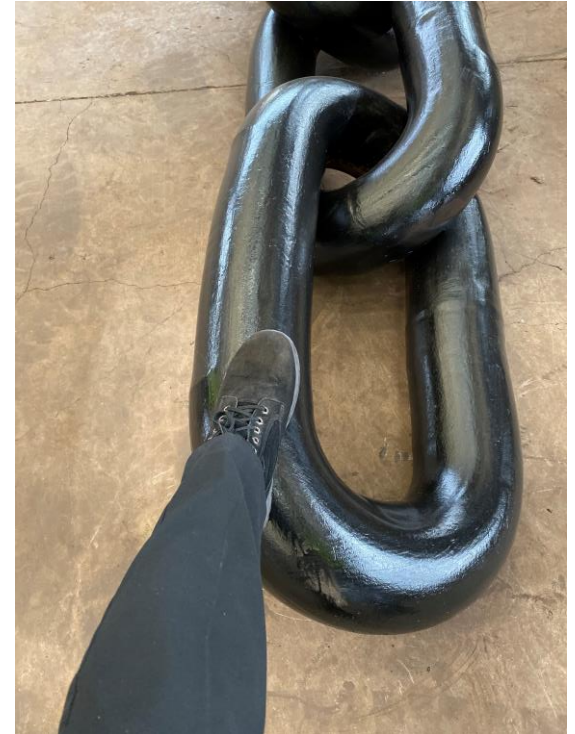


Product Complexity

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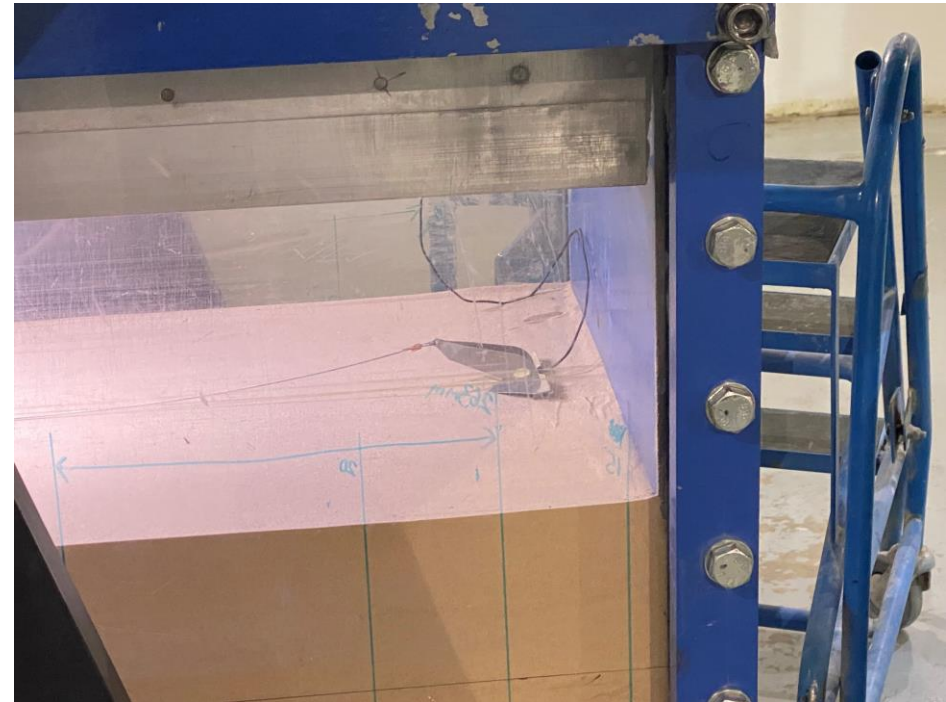
MOORINGS AND ANCHORS



Planned Production Possibilities



Planning ahead – R&D



Planning ahead – R&D

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MOORINGS AND ANCHORS



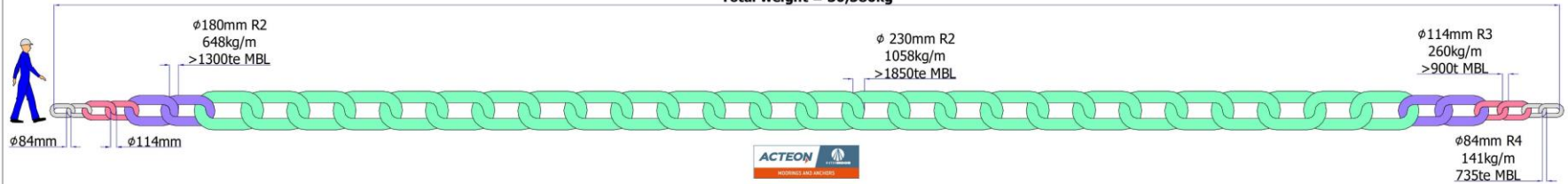
Planning ahead – R&D



30m of InterMoor Transition Mooring Clump Chain

- consisting of:
- 4x $\phi 84$ mm links
- 4x $\phi 114$ mm links
- 4x $\phi 180$ mm links
- 26x $\phi 230$ mm links

Total weight = 30,580kg



THANK YOU

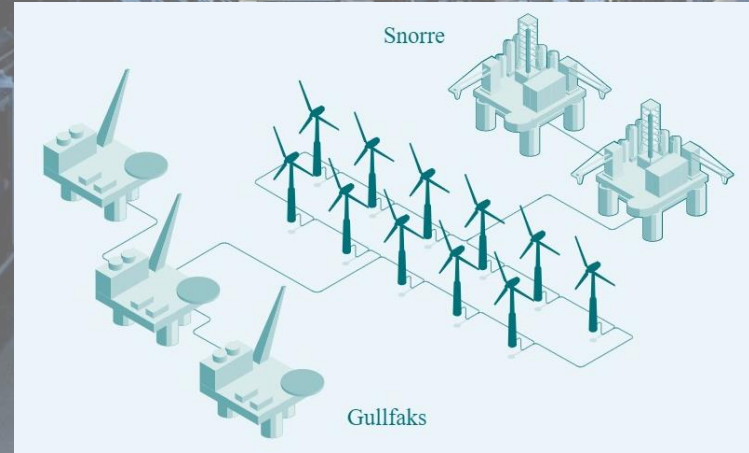
Hywind Tampen - Mooring Experiences

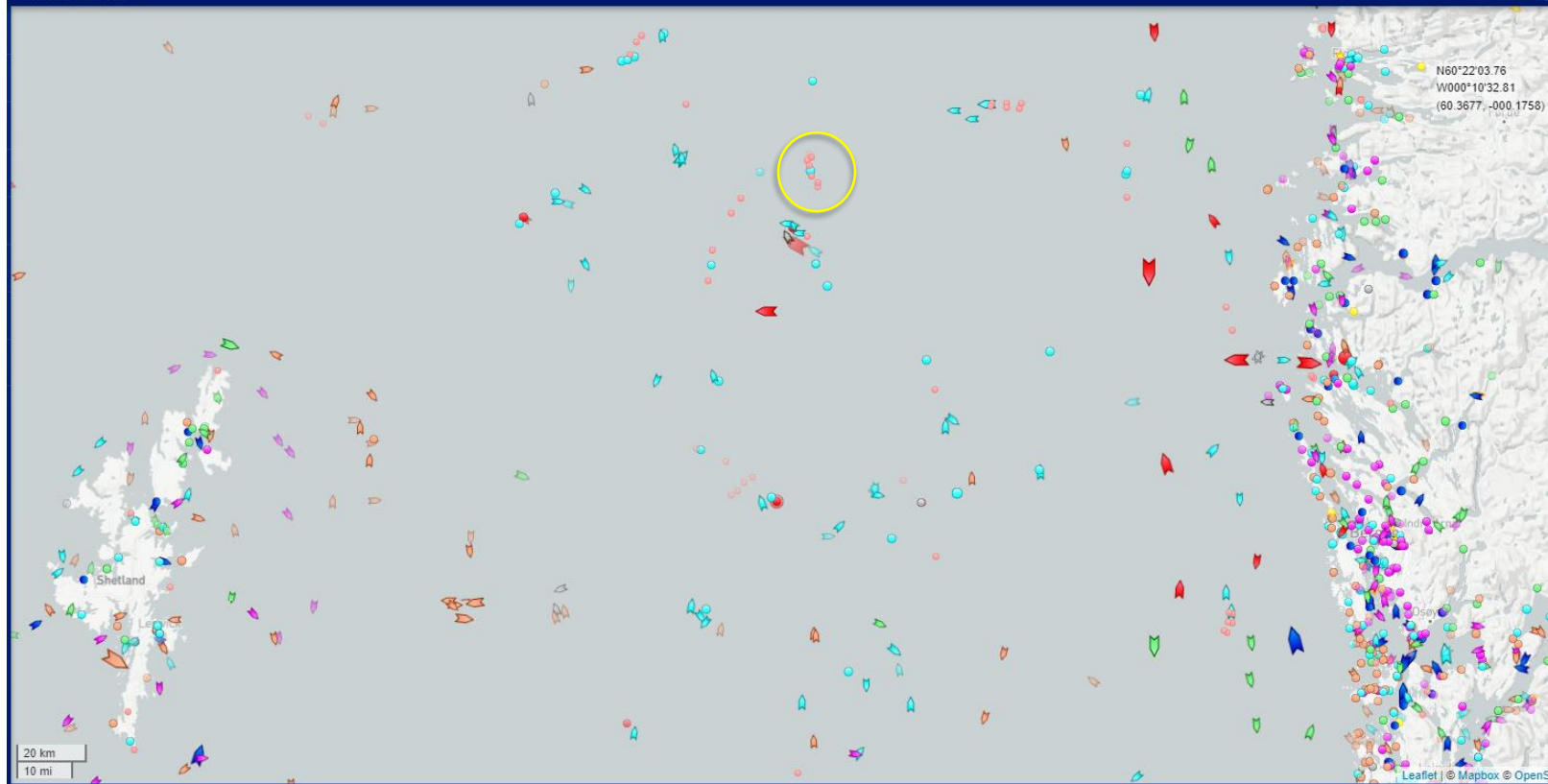


Hywind Tampen Project

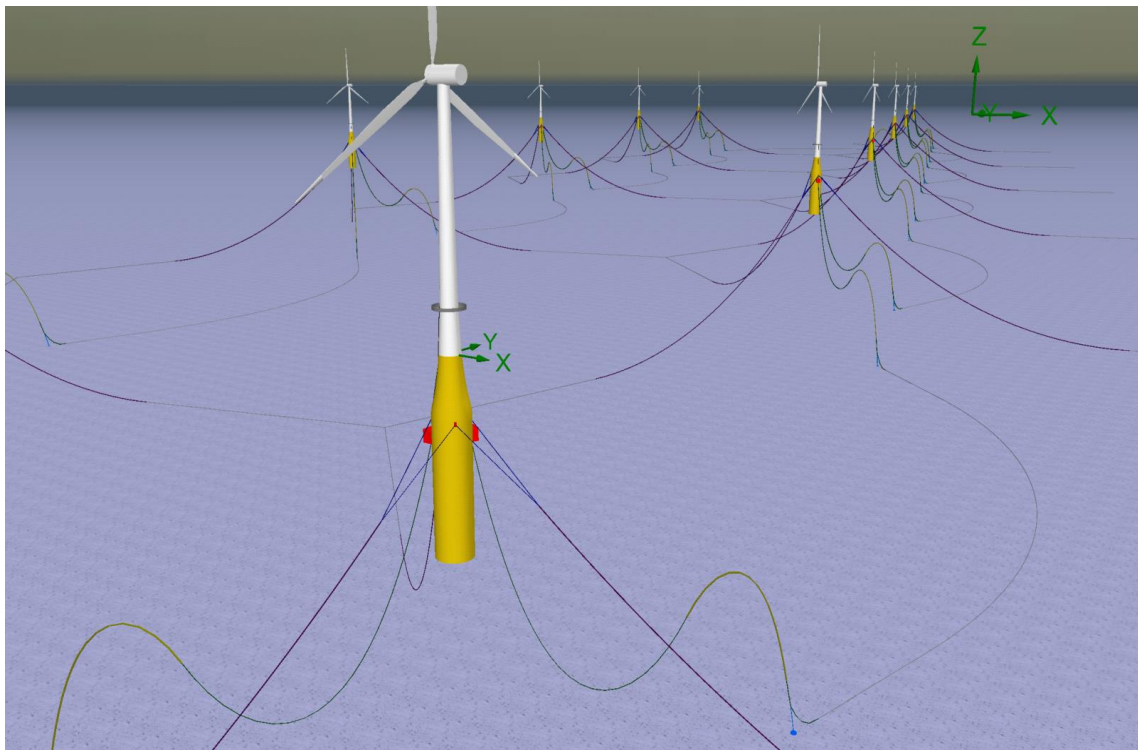


- **Hywind Tampen** at 95MW will be the world's largest floating offshore wind farm and an essential step in industrialising solutions for future floating wind farm projects





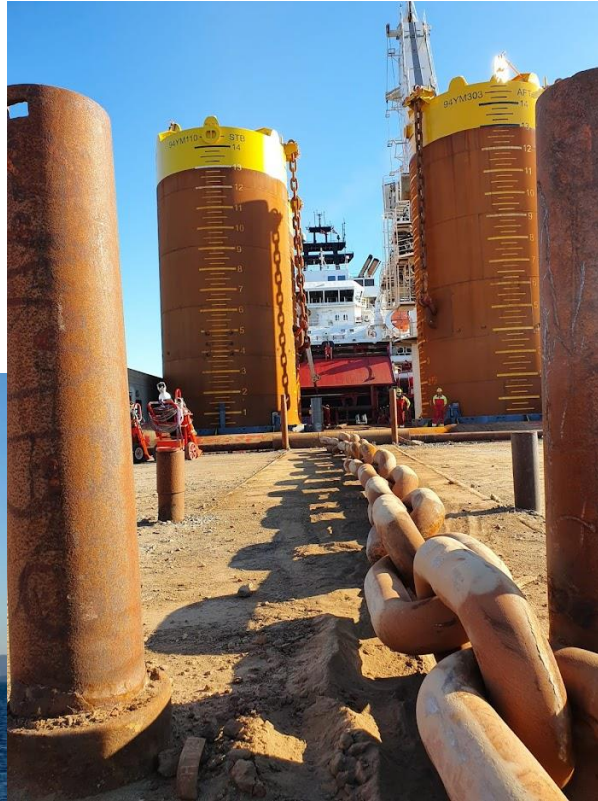
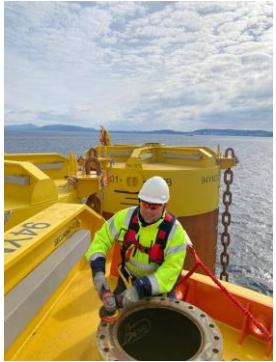
The mooring layout



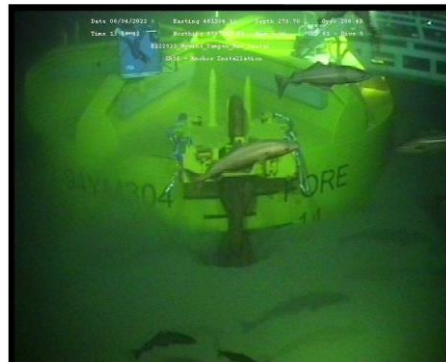
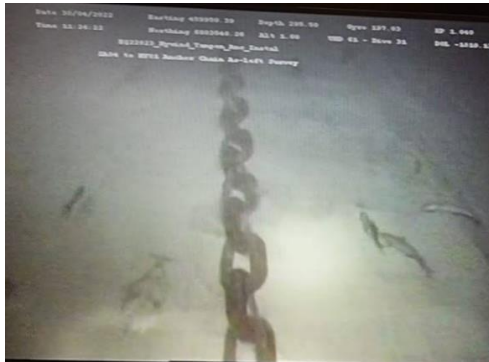
- 2 passive and 1 active line for each turbine.
- Active line with an in-line tensioner.
- Lines are SSSW and Bottom chain.
- 19 suction anchors 33 mooring lines (avg 1.7 suction anchors/turbine).
- Anchor and chain installation (and tensioning) took 43 days incl. weather.

Mooring system load-out and FWT assembly site

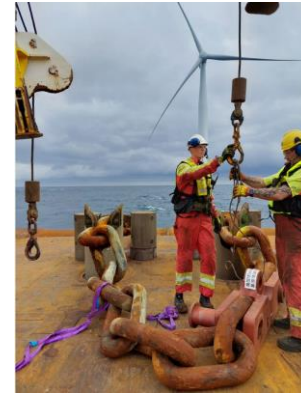
Mooring system - load out for installation



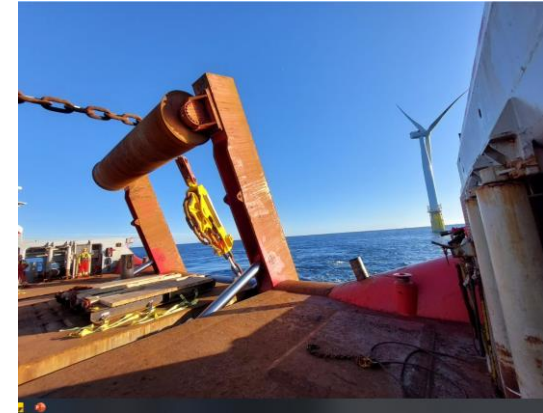
Mooring Installation



Tow out and hook-up



- Spread. 3 towing and 1 installation vessel.
- Skandi Iceman «a-frame» used for In-Line Tensioner installation. ILT launch. working well.
- Hook-up operations combining several vessels with system under tension. Not ideal, time consuming and fragile method. Fabrication (of substructure), installation, operation and maintenance should get more focus when designing the mooring system.
- Soil and water depth will vary but within some areas there should be optimisations. Oil and gas moorings are one off, robust but expensive.
- Hook-up and installation time has to and can come down. 60 days for 7 turbines. (logistics, weather and method)



Some lessons learnt

1. To get a **good mooring design, more experience**, data collection and data sharing will be important.
2. The **contracts** for floating wind development must be **better adapted to the work** and **clear interfaces** must be established. **Lump sum contracts** are often used. That format is **not ideal**, as the product and interfaces are unclear and not established. Focus should be on paying for added value. With LS the focus becomes, get it done as easily as possible (and the big picture is forgotten).
3. The **installation time and weather criteria** for mooring systems **need to improve**.
4. More **specialized and cleaner vessels**, to be developed once we have sufficient experience. Long term contracts for vessels will be an advantage for all.
5. Experiences from **oil and gas is relevant and very useful**. However, the **organizing** needs to be more **flexible** and should be more **«IT driven»**. **Matrix organizations with departments are not ideal** for these development projects where the way forward, roles and responsibilities are under development and constantly changing.
6. **Unforeseen changes** will come and make a major impact on projects. Examples from Hywind fuel price, tax regime, Covid, supply chain constraints etc.
7. **Offshore vessels can be unreliable**, the mooring campaigns over 4 months had vessel breakdowns three times requiring replacement vessels.

Thank you





BAUER Offshore Technologies GmbH

Marine Foundations installation

Floating Offshore Wind Subgroup

Transitioning from current areas & business

Transition opportunities

Bauer Universal Mooring Pile

Scaling up for commercial array FOW
In any combination of soil, clay & rock

Bill Shaw: Commercial Director
BAUER Renewables Ltd



In addition to our century-long drilling expertise on land, BAUER has also gained significant experience offshore since 1993



BAUER Offshore Project History

Diamond deposit exploration with a BC Cutter in water depth of 160 m (South Africa, Atlantic Ocean)



1993

Barrow Offshore Windpark: Drilling inside of a monopile with a Bauer Fly Drill (Barrow / UK, East Irish Sea)



2008

Relief drilling for driven pin piles with Dive Drill, commissioned by Seaway 7 (Beatrice OWF / UK, North Sea)



2017



First MeBo Worldwide sea bed core drilling (©MARUM – Center for Marine Environmental Sc., Bremen)

2011/12



Monopile foundation in rock for tidal turbine from Voith Hydro with BSD 3000 (Orkneys / UK, Atlantic Ocean)

2021-2023



Provision of drilled & grouted pin piles with Dive Drill, (St. Brieuc OWF / France, Atlantic Ocean)

Bauer Offshore Project Recent History



2008 . Barrow Offshore Windpark, UK

The monopile foundations for the 90 MW windpark in the East Irish Sea were installed by the Drive-Drill-Drive technique. Bauer performed the relief drilling using the **Bauer Flydrill BFD5500**. The frictional resistance was reduced for the 4.75 m diameter foundation pieces in the hard soil layers.



2011 – EMEC Monopile – Tidal Turbine – Orkney, UK

Bauer was the principle contractor for the monopile foundation of a tidal turbine from Voith Hydro.

The drilling equipment was the **Bauer BSD3000**. Able to operate in 12 Knots current and drill hard rock – uncased

Water Depth = 37 m
Monopile Length = 23 m
Monopile Diameter = 2 m
Rock Socket Depth = 11 m



2017 – Beatrice OWF, UK

Bauer was commissioned by Seaway 7 to provide relief drilling services for driven pin piles.

The drilling equipment was **Bauer Dive Drill – DDC 40**

- 3m diameter
- 70m penetration
- 40m water depth
- Standby use based on pile hammering refusal



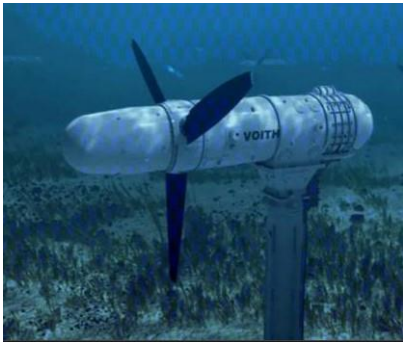
2021 to 2023 – St. Brieuc OWF, France.

Bauer is contracted by Van Oord to provide drilled & grouted pin piles

The drilling equipment is **Bauer Dive Drill – DDCU 40**

- 62 WTG / 1 OSS
- 190 Pin Piles
- 3m diameter
- Up to 47m penetration
- +40m water depth

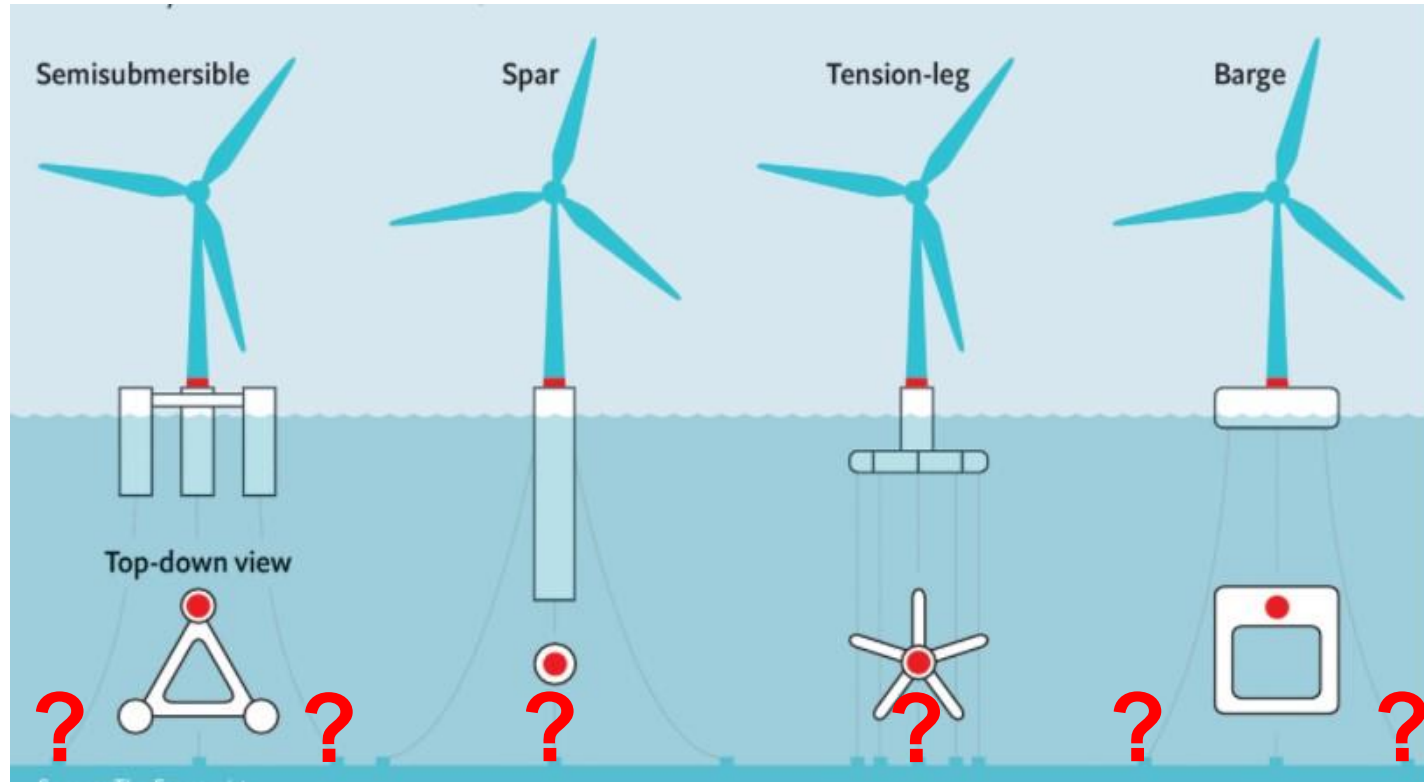
BAUER Offshore Foundations



Scottish HQ - Dundee

Floating Offshore Wind – Foundation fixation choices – where to start?

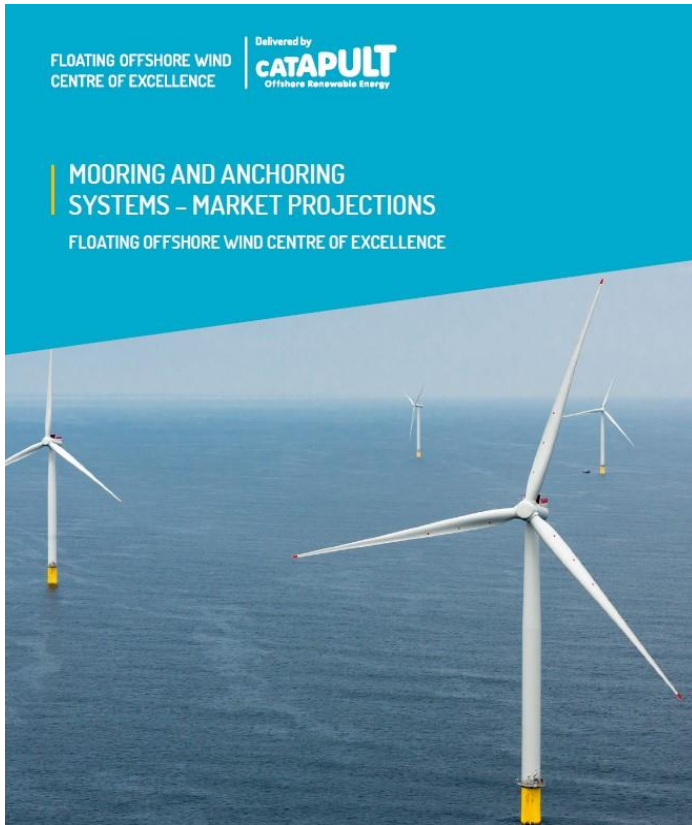
You start with geology – and if geotechnically it is difficult, what then?



Difficult Seabed Geology

Anchor type	Type of seabed
	1. Outcrops and seabed surface rock 2. Medium & hard sub rock layers interspersed with cohesive & non cohesive soils 3. Any combination of any seabed soil/ rock
Gravity-base anchor	? Requires seabed preparation – uneconomic @ scale & often not possible
Drag-embedded anchor	X Ideal in cohesive and non-cohesive soils – some capability in hard soils but limited to fluke contact in soft limestone and coral
Driven pile anchor	X limited to <5Mpa soil strength – ideal in soft cohesive seabed
Suction anchor	X ideal in soft cohesive seabed
Driven anchor plate	X ideal in soft cohesive seabed
Torpedo embedded anchor	X ideal in soft cohesive seabed
BAUER Drilled and grouted pile anchor	1, 2 & 3 Yes - BAUER install D & G piles in any seabed material in any combination and thickness, from 1 Mpa overburden to 200 Mpa rock in any layer thickness & combination thereof. 5-50m long piles & 2 to 4m Ø

Are there disadvantages with D & G piles?



- Drilled and grouted piles
- : 4.1.4: *may be the only option for some seabed conditions.*
- But they can be costly? Right!



No escaping big ticket items when working at sea, however with target prices well below that for similar works in other marine sectors, then no, this is now not the case for FOW.

But how do we reduce serial costs to acceptable levels?

Floating wind needs to focus on cost and risk reduction

(IRENA – International Renewable Energy Agency)



We need to use Smaller vessels

- Lower cost
- Better Availability
- Faster more agile installation

We must Standardise wherever possible

- Utilise same equipment spread every project
- installing same pile \varnothing for any project - Just adjust drill depth

We must Optimise design & installation phase

- Pile sharing for catenary mooring – more efficient
- Bigger Turbines – using high-capacity D & G piles
- Bigger arrays – more opportunity - reduce serial cost

Higher ROI at much lower risk – yes please!

But how will we do this?



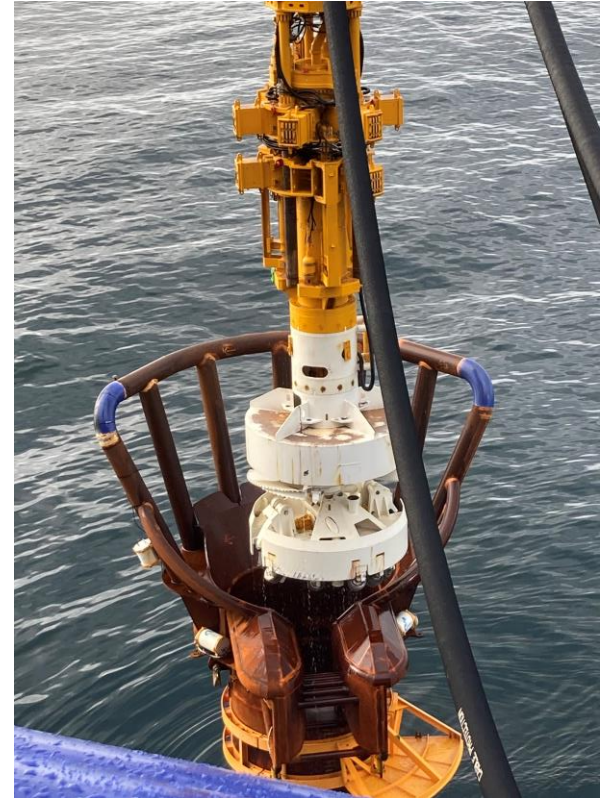
It takes experience, knowledge, resource and clever design



BAUER are now offering to all Scotwind FOW partners, fast and economic installation of high-capacity mooring piles that will de-risk projects in hard soils and rock – and make them financially attractive.

Thank you and Questions

Please contact Bill Shaw for more information:
Bill.shaw@bauer-renewables.co.uk



*PASSION for
PROGRESS*

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DeepWind FOW Subgroup Event – Mooring Systems

Ferdinando Samonà – Floating Wind Engineering Manager

Glasgow, 23/08/2022

A Green Transition at Maersk Supply Service

Our green technology and solutions

Floating wind

End-to-end solutions
with tailored work scopes



Stillstrom

Electric charging
power buoy technology




Vertical Installer

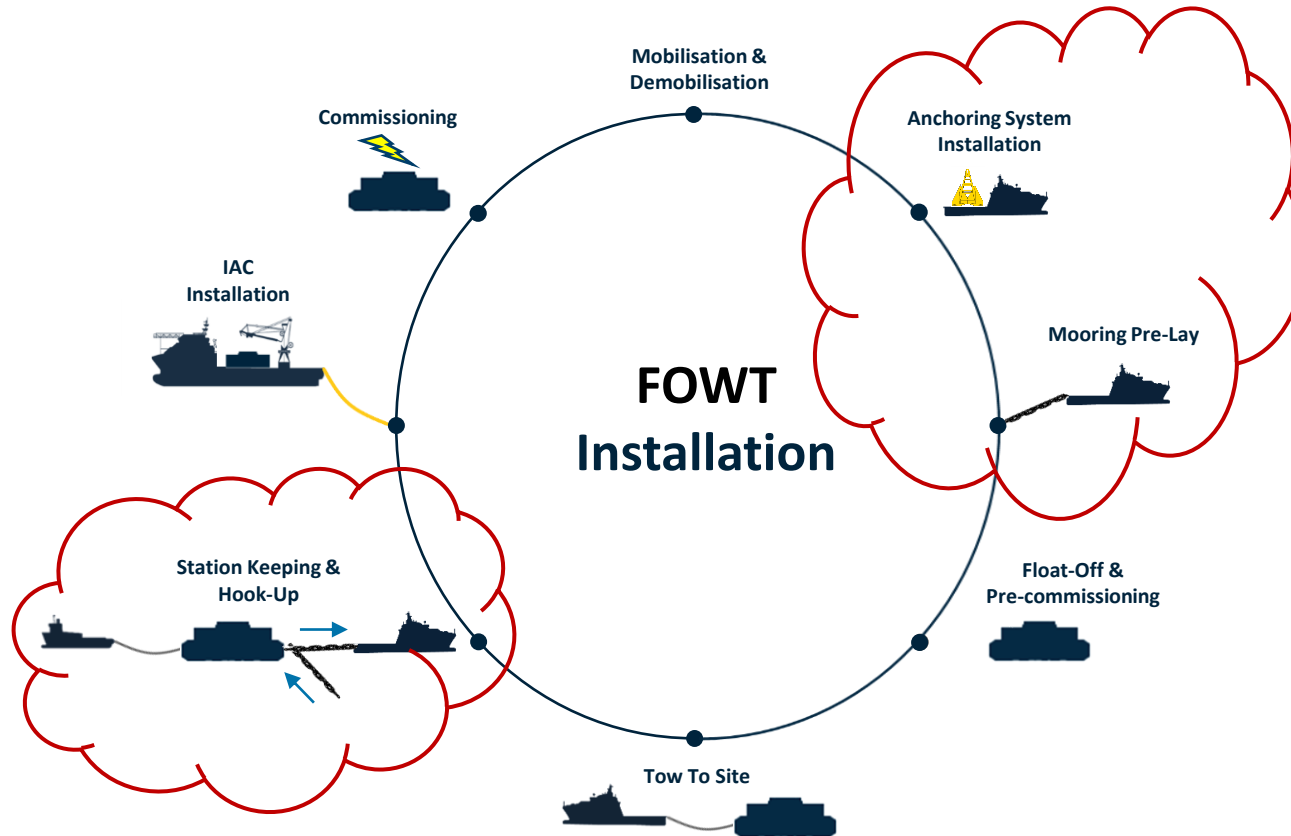
Innovative solutions for
wind turbine installation



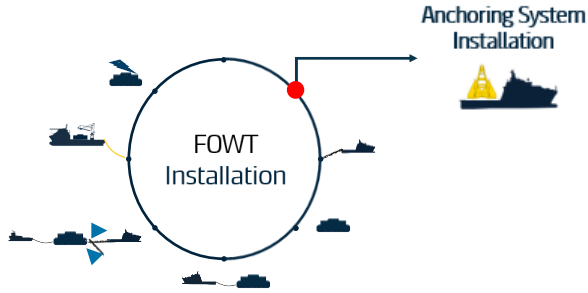
Mooring related topics of Today's Event

- Mooring component manufacturing
- Marshalling and load out
- Mooring Systems Installation 
- Innovations related to mooring and anchoring systems for FOW

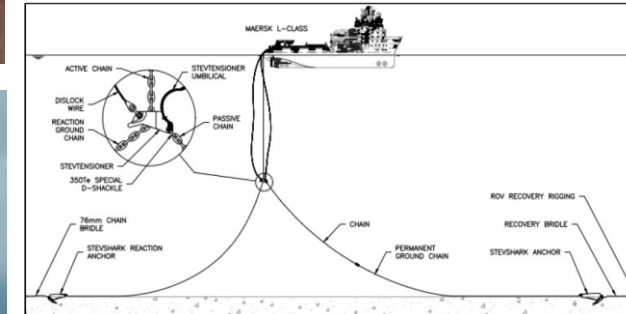
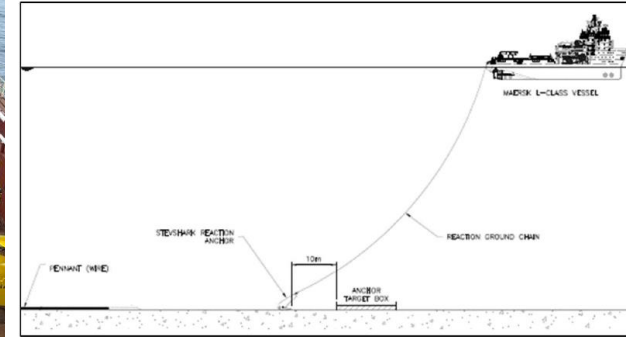
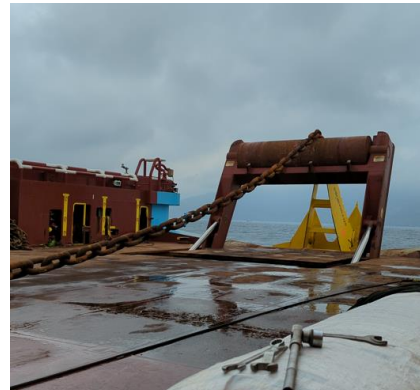
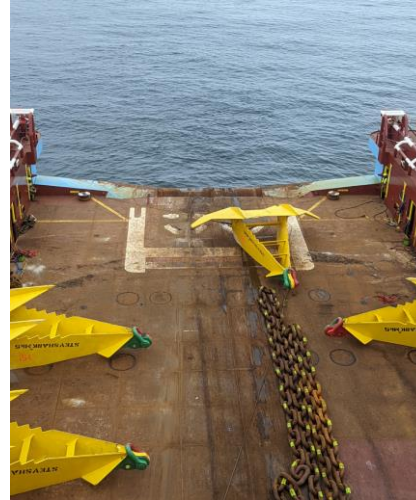
FOWT Installation - Typical Installation Sequence



Anchoring System Installation

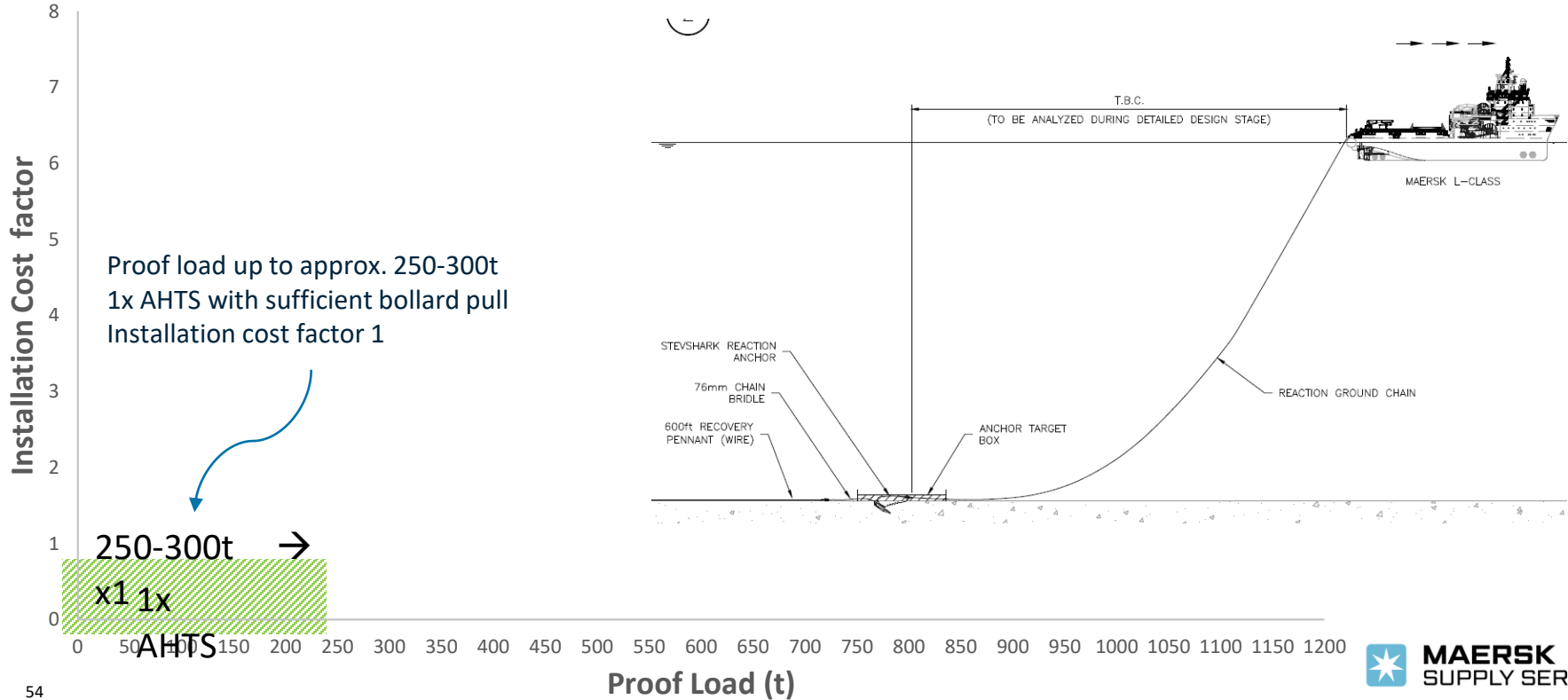


- Drag Embedment Anchors (DEA), Suction Piles, Driven Piles, Drilled-Drilled/Grouted Piles, Deadweights, etc.
- DEAs require to be proof loaded offshore.
- The proof load shall be equal to the max. line tension under extreme conditions (Ref. DNVGL-OS-E301 Ch.2 Sec. 3.6.2).
- How does the proof load influence the selection of suitable marine asset and what can be the impact on installation costs?

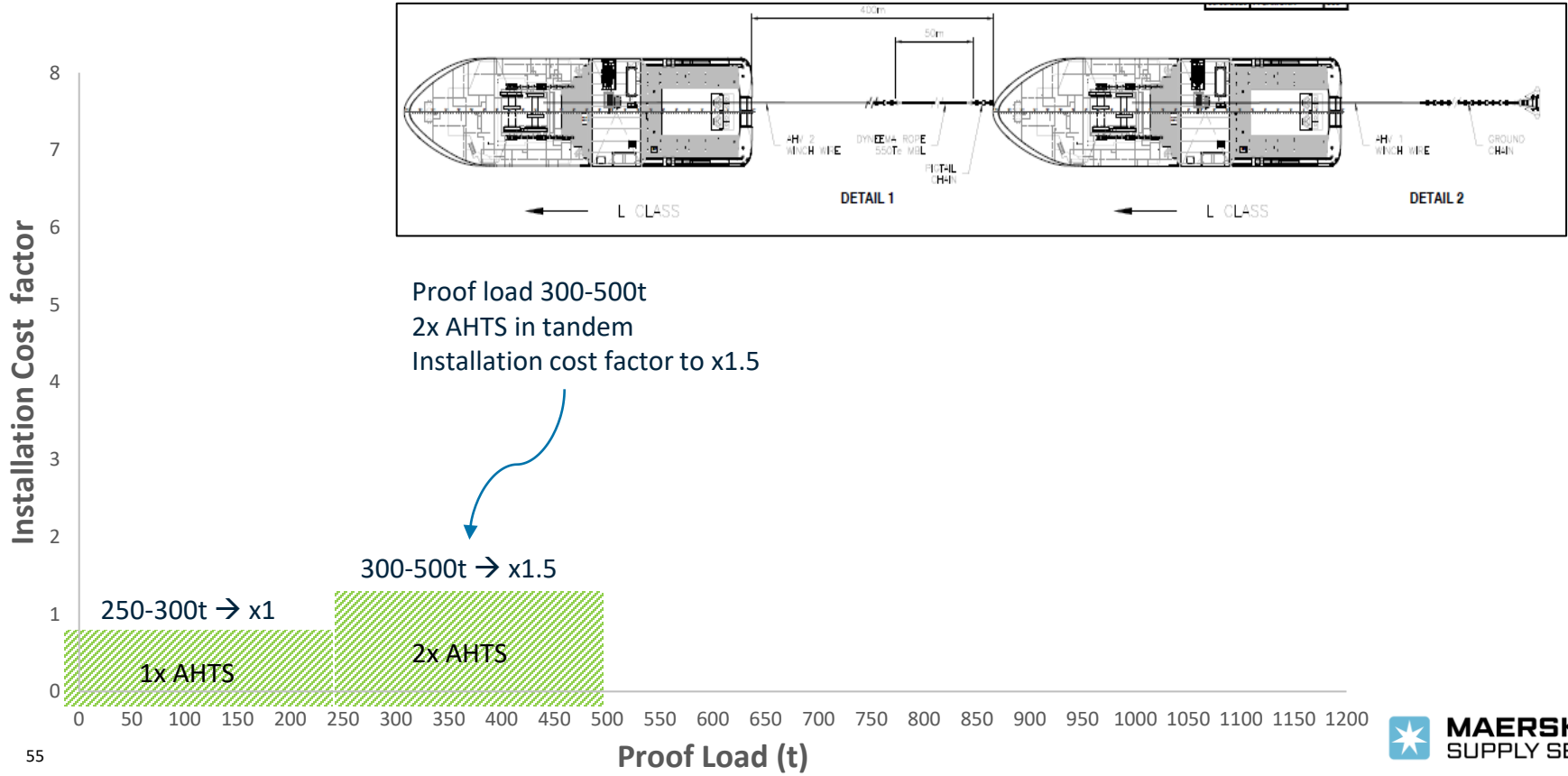


DEA Installation – Proof Load VS Installation Spread

- Installation costs depend on various parameters and specific assessment is required on a case-by-case basis
- Example below refers to a FOW Demo project in a water depth of 60-80m



DEA Installation – Proof Load VS Installation Spread



Proof load 300-500t
 2x AHTS in tandem
 Installation cost factor to x1.5

300-500t → x1.5

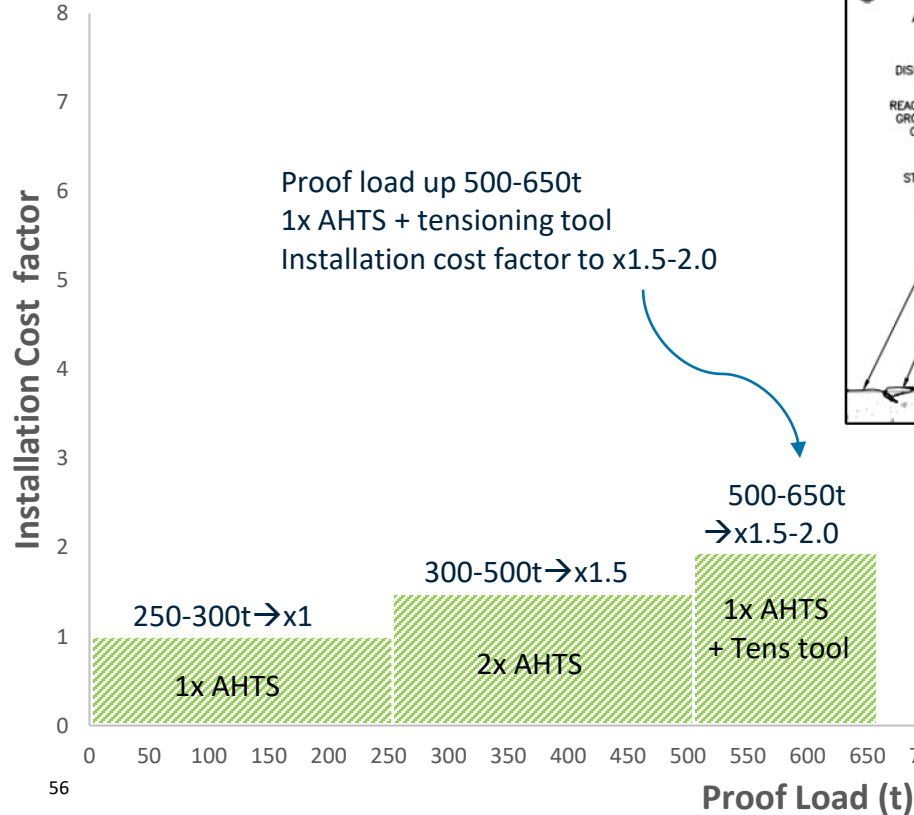
250-300t → x1

1x AHTS

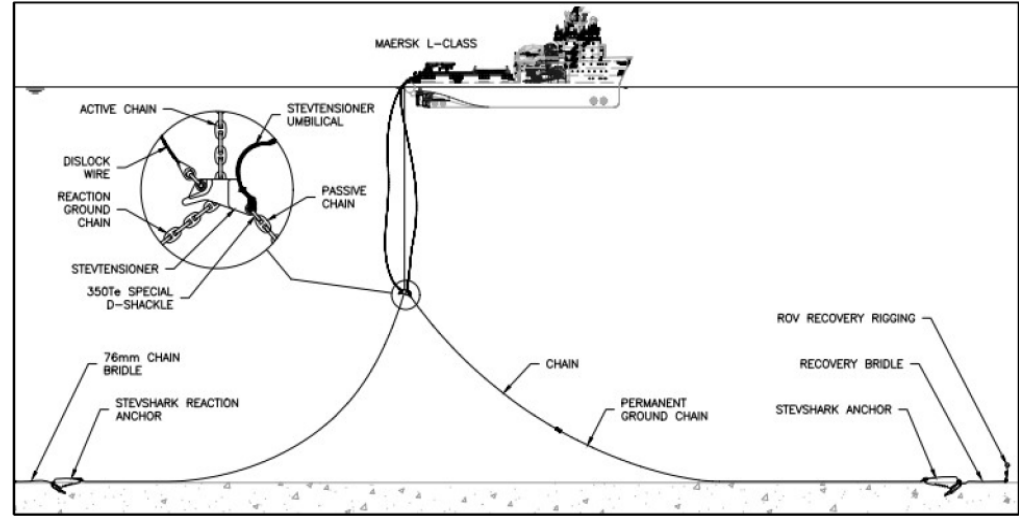
2x AHTS

Proof Load (t)

DEA Installation – Proof Load VS Installation Spread



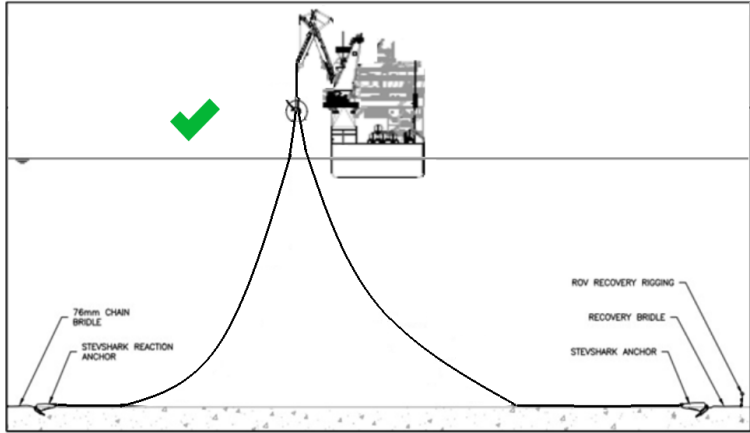
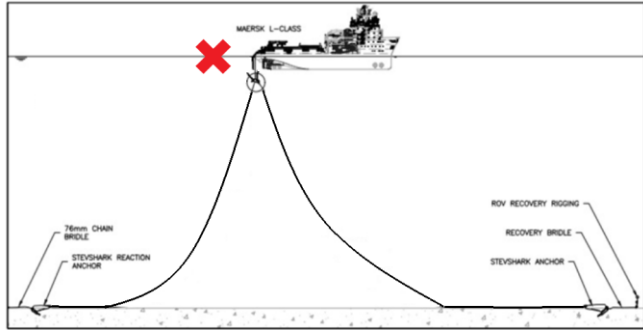
Proof load up 500-650t
1x AHTS + tensioning tool
Installation cost factor to x1.5-2.0



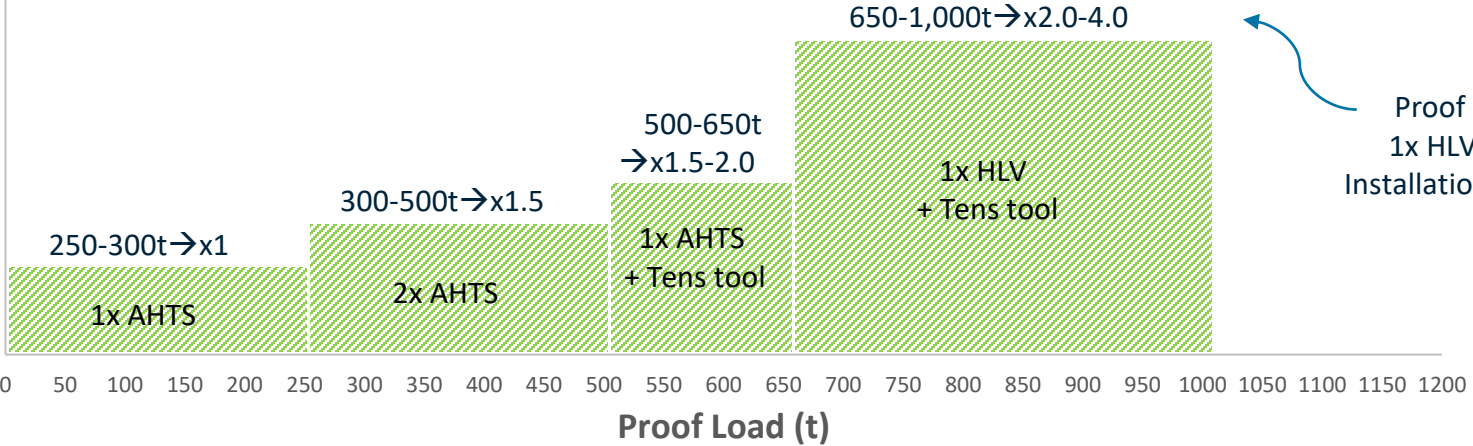
*Approx. 40% of vertical pull is required to achieve the proof load – e.g. 500t vertical (applied via main AHTS winch) can achieve 1,200t horizontal.
So why only up to 650t?*

DEA Installation – Proof Load VS Installation Spread

Insufficient water depth, tensioning tool to be lifted above sea surface



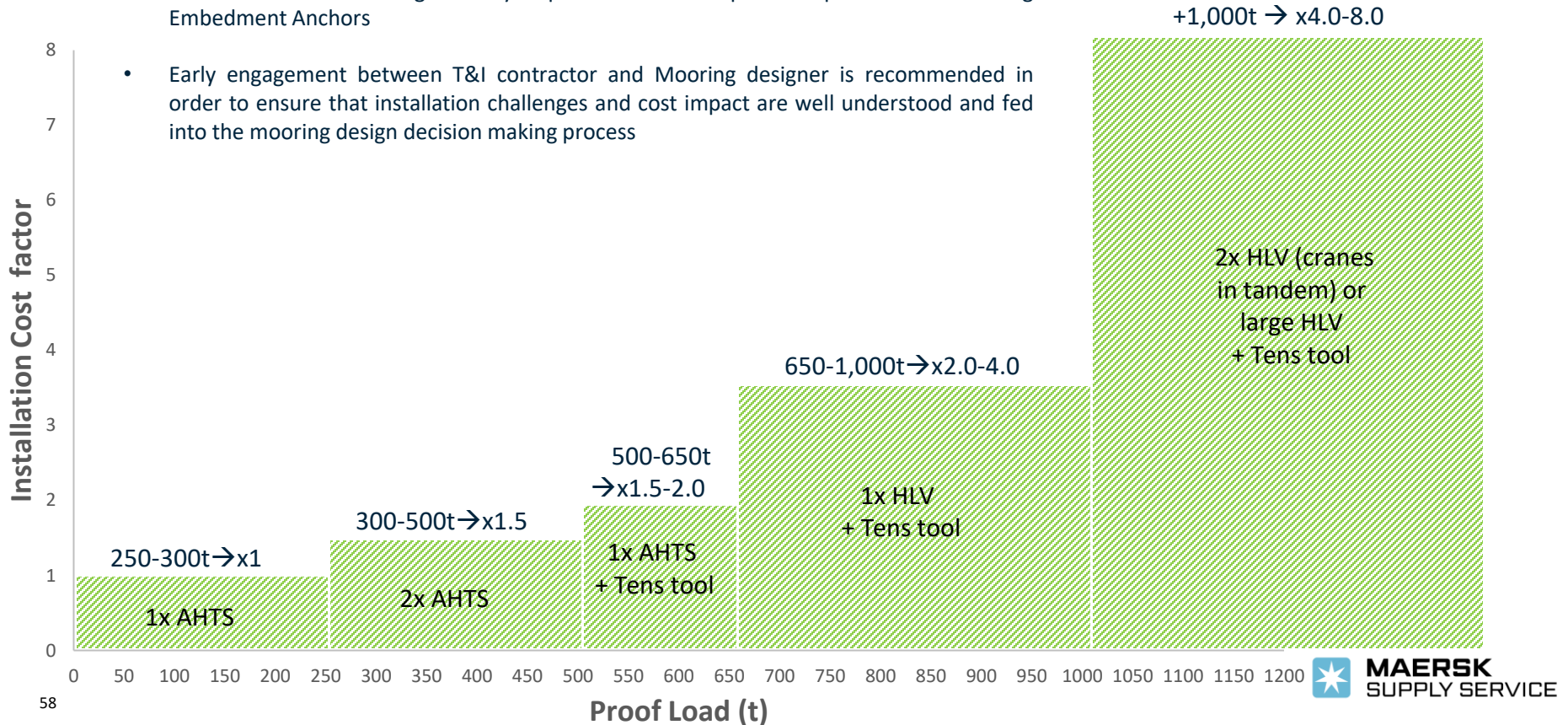
Installation Cost factor



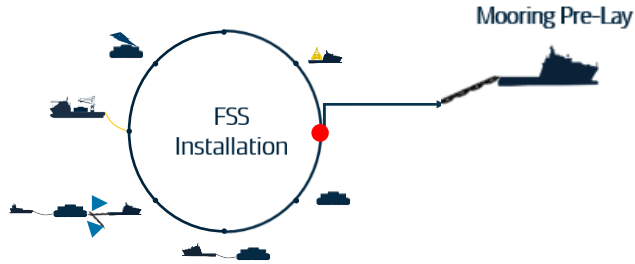
Proof load up 650-950t
1x HLX + tensioning tool
Installation cost factor x2.0-4.0

DEA Installation – Proof Load VS Installation Spread

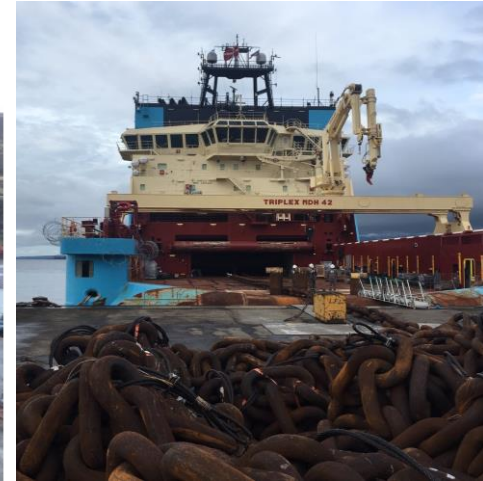
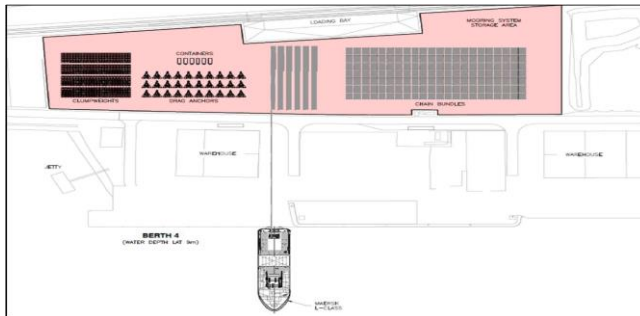
- Proof load values can significantly impact the marine spread required to install Drag Embedment Anchors
- Early engagement between T&I contractor and Mooring designer is recommended in order to ensure that installation challenges and cost impact are well understood and fed into the mooring design decision making process



Mooring Installation – Pre-Lay

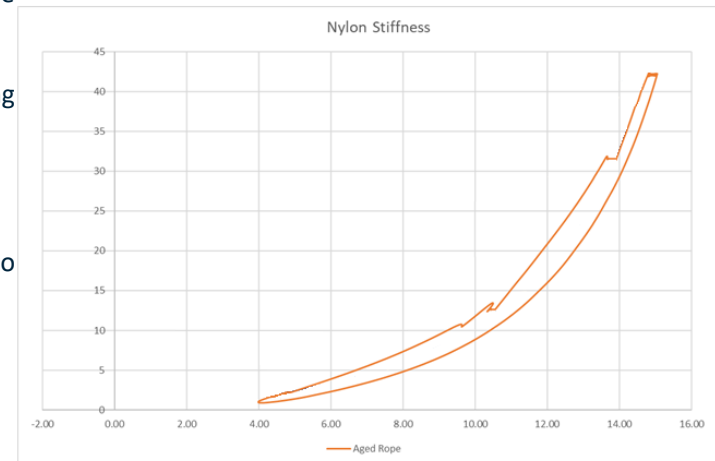
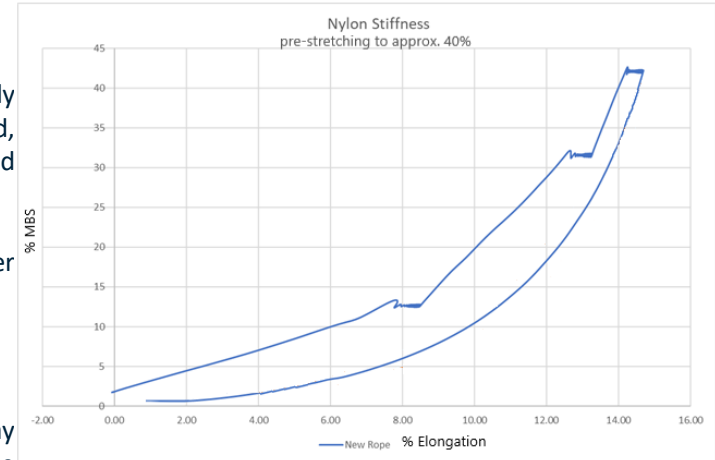


- Pre-lay of chains, ropes and connectors
- AHTS with sufficient chain locker space, deck space, bollard pull and winch capacity required
- Synthetic rope pre-stretching operation may be required to remove construction elongation
- New synthetic lines/ropes should be pre-stretched as stated by DNV-ST-N001 Sec 17.8.6.4



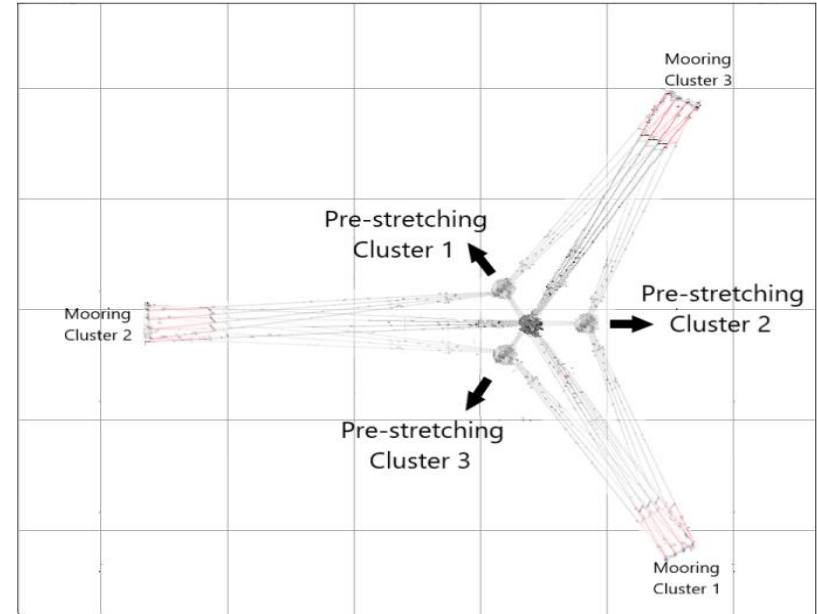
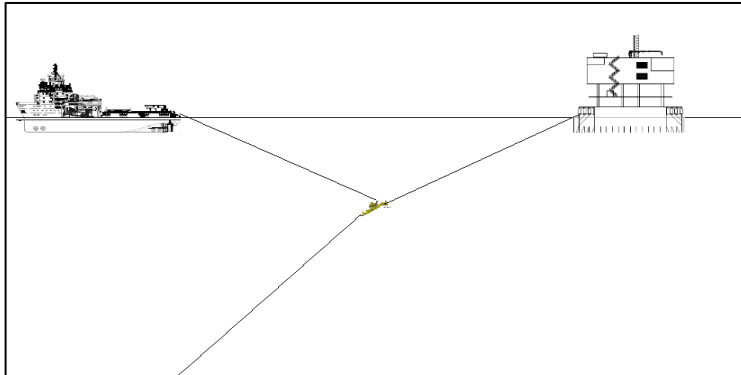
Mooring Installation – Synthetic Rope Pre-Stretching

- New synthetic ropes are characterised by construction elongation and creep
- Construction elongation is a temporary elastic elongation which can be temporarily (and partially) removed by applying and holding tension. If the tension is removed, then the rope will almost fully retract back to its original length (e.g. removed construction elongation <1% on nylon rope)
- Creep is a permanent plastic elongation which will only be removed over time under long term loads
- Synthetic ropes stiffness stabilises over few years of operating life (aged rope)
- Because of these elongations, in the first few years of operating life new ropes may lead to higher Floater excursions than the capacity limits of the dynamic cable if the elongation is not carefully handled.
- For the above reasons, pre-stretching of a new rope (i.e. accelerating ageing process) may be required
- But is pre-stretching always worth it?
- E.g. is it worth pre-stretching before the hook-up and then wet-store the rope onto seabed?



Mooring Installation – Synthetic Rope Pre-Stretching

- Unless the tension is kept high after the pre-stretching, significant construction elongation will still be expected after hook up
- Creep will only be removed over time under long term load and are unlikely to be removed during pre-stretching operations
- *Feedback from a rope supplier is that the elongation that is eliminated with a pre stretched nylon rope at 40% MBS and then removing the tension versus a non-pre stretched nylon rope can be as small as approx. 0,5%*
- In Oil & Gas industry, accelerated ageing is typically achieved by cross-tensioning the ropes after the hook-up using large tensioning equipment onboard the platforms i.e. the minimum tension seen by the rope after pre-stretching is the mooring pre-tension
- In FOW generally there are not large tensioning equipment onboard the Floater, hence this can only be done with suitable marine spread in combination with permanent subsea tensioning tools such as ILTs, chainstoppers, etc. (requiring a certain length of permanent chain)



- Due to the large ropes used in FOW applications (e.g. MBS of 2,500t), pre-stretching loads introducing significant technical and commercial challenges. The need of pre-stretching should be carefully assessed and alternatives investigated
- Careful attention to balancing the elongation effects with the mooring and cable design is required together with an intervention which may require re-tensioning activities until the rope elongation stabilises

Thanks

Further questions? please contact:

Ferdinando Samonà – Floating Wind Engineering Manager

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Phone: +45 3178 1026



Structural Health Monitoring Floating Offshore Wind Turbines

DeepWind – Floating Wind Subgroup

Stuart Killbourn, 23 August 2022



Floating Wind: Fatigue Tracking

Motion and position measurements of floater are interpreted using a physics-based simulation model to infer stress cycles – hence **fatigue**.

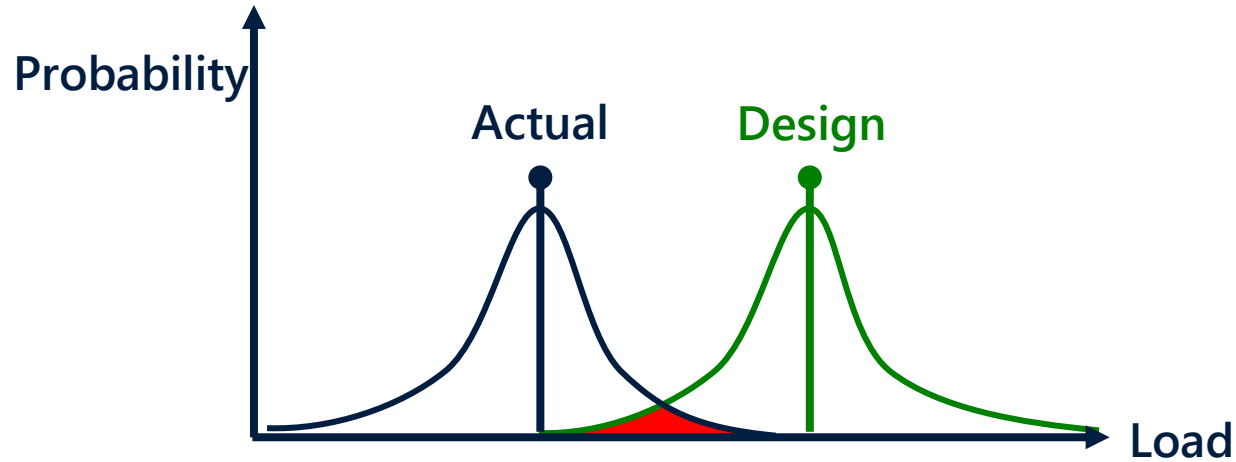


Objectives:
Reduce or **Eliminate**
Subsea Inspection.

Utilise **Dry, Robust,**
and **Maintainable**
Instrumentation for
low operating costs.

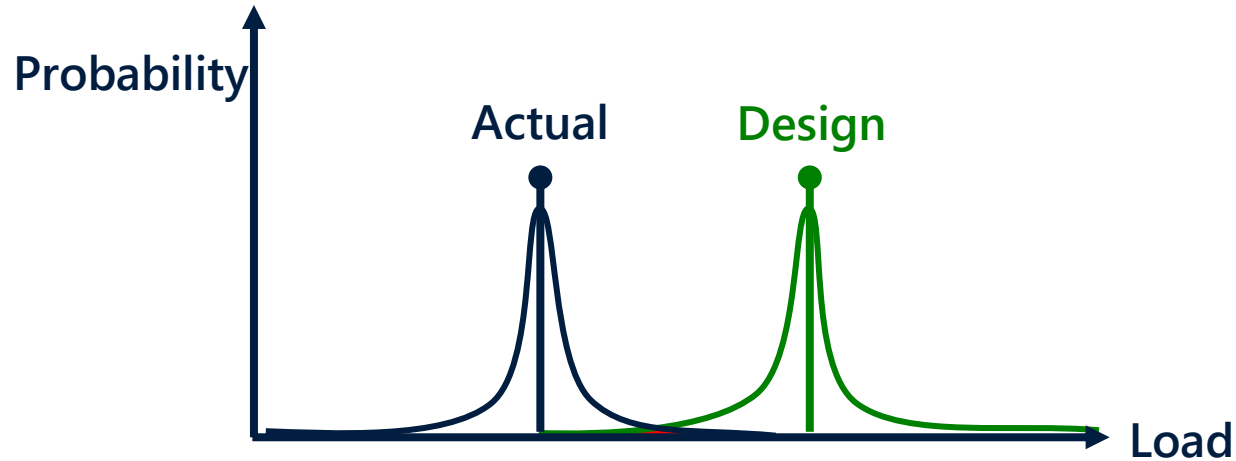
Continuous **anomaly**
detection for anchor
drag or similar failure
scenarios.

Risk-Based Inspection

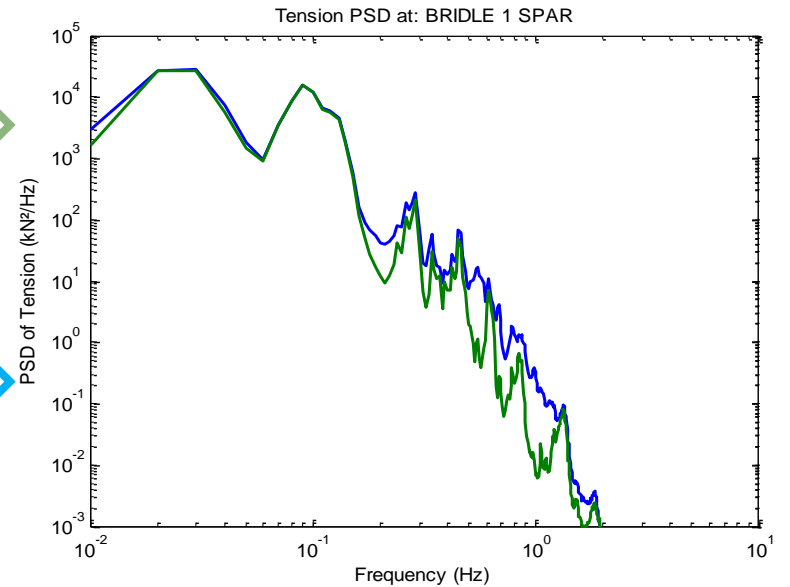
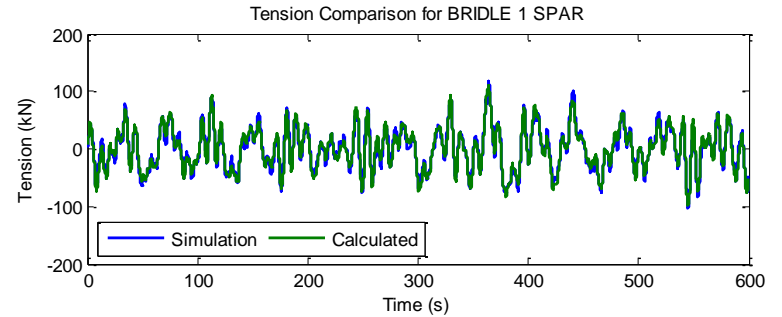
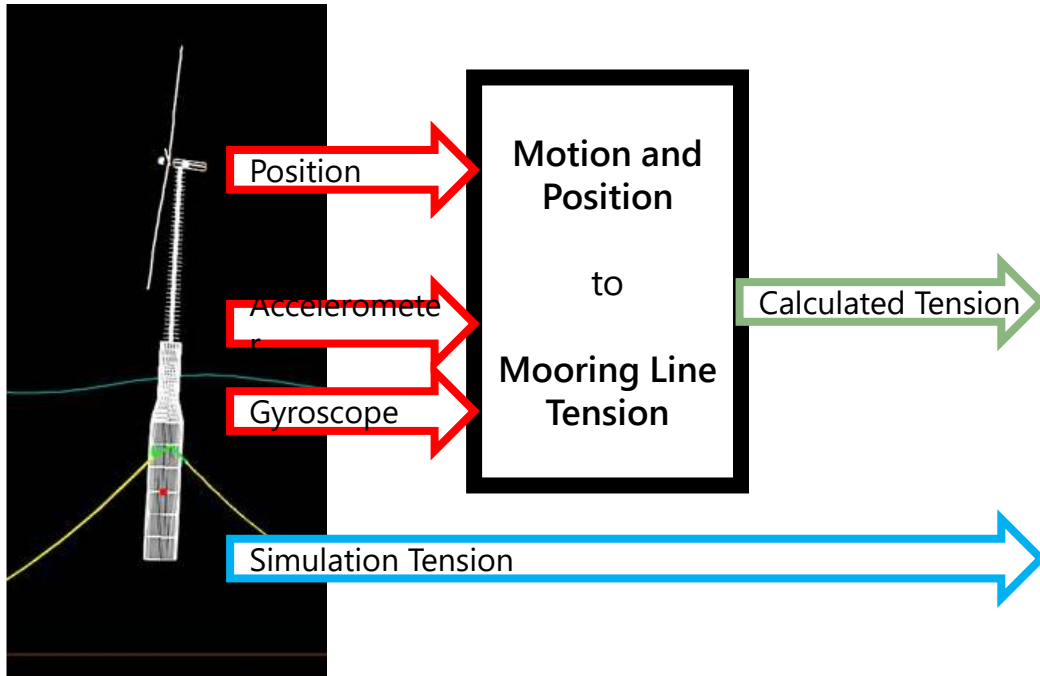


Risk-Based Inspection

Better information allows us to quantify the risks more accurately – and target inspection efforts.



Mooring Line Tension



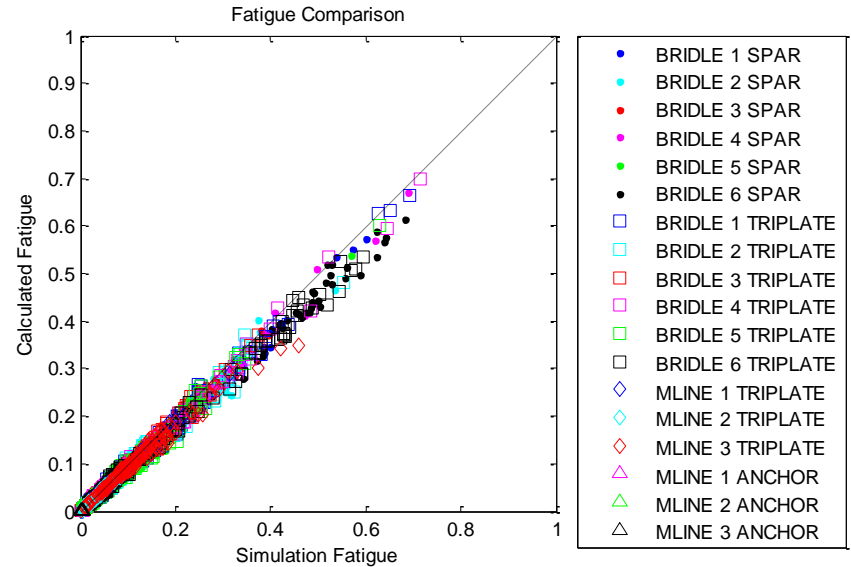
Verification: Fatigue

Verification results from Hywind Scotland simulation model show excellent correlation.

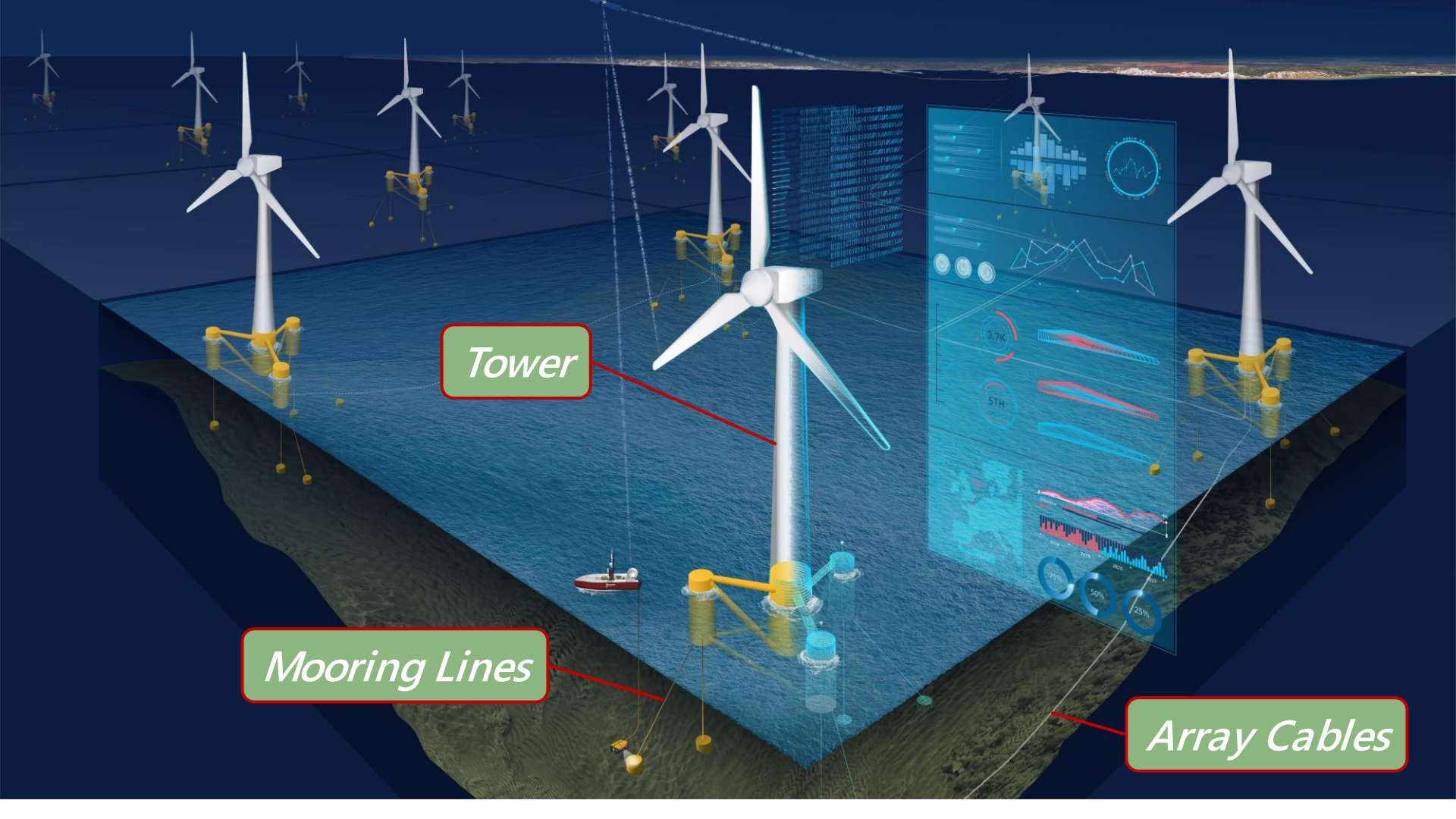
Promising results using limited Hywind Scotland published data set.

Next step: validate results in a field trial:

- Install monitoring system on FOWT
- Create simulation model
- Track fatigue with sensor data as input
- Ideally compare versus load cell



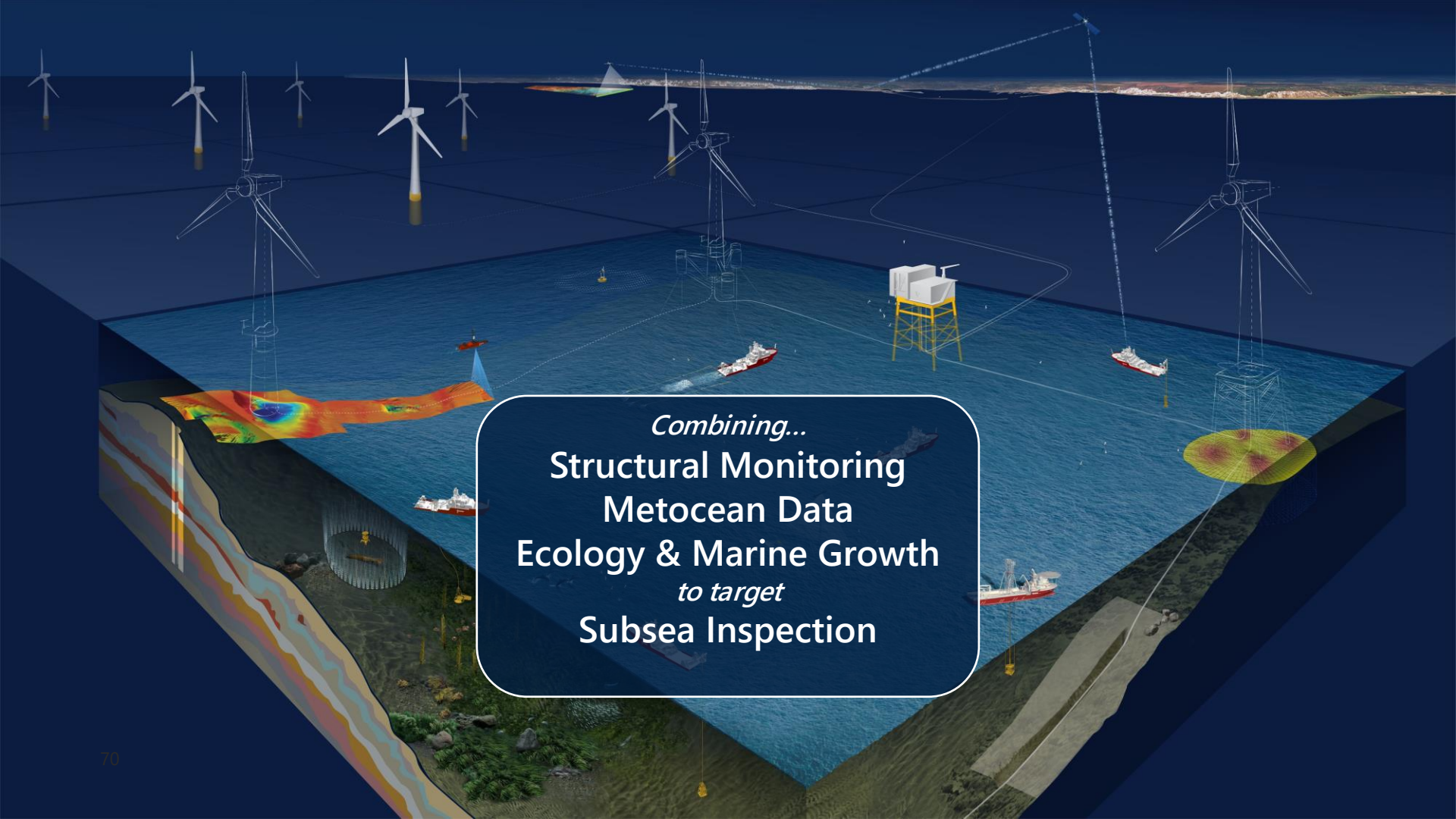
Typical fatigue ratio is 0.9.
10% error in fatigue
(or 4% error in stress cycle range).



Tower

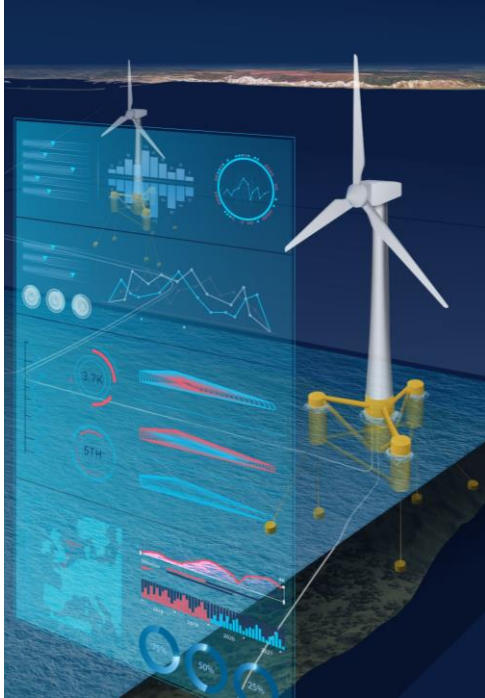
Mooring Lines

Array Cables



Combining...
Structural Monitoring
Metocean Data
Ecology & Marine Growth
to target
Subsea Inspection

Conclusion



Remote monitoring of floating wind turbines is a cost-effective, un-manned solution to asset integrity that enables:

- Life extension
- Inspection and intervention optimisation
- Identification of damage or failure scenarios



Thank you

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 fugro.com

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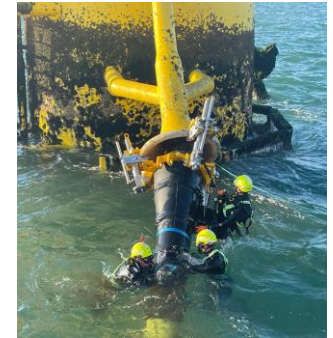
LESSONS LEARNT & CHALLENGES

Cable Operations



Preventing Maintenance
Cable Protection
Site Conditions

Bio-fouling



Subsea assets have gain close to 1t
worth of marine growth.

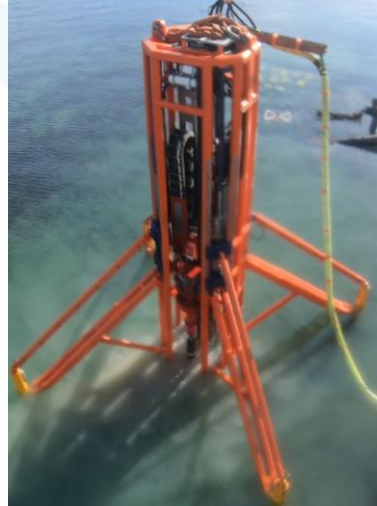
Mooring Operations – R&D

Mooring solutions

Gravity Bases
100T-300T



In 2019 we source and installed a total 1200t of chain to work as mooring system

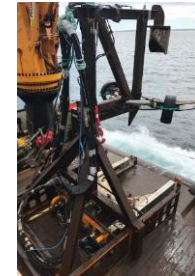


The SDR project is the design, manufacture and development of cost-effective drilling option for mooring and anchoring solutions. This project augments the existing drilling rig concepts available on the market with an innovative, robust purpose-built solution that will enable low-cost drilling & piling operations.

Leask Marine
Raptor SDR



Continue Developing...



BBRG Synthetics

Preparing for Scotwind

Stein Are Andersen

23.08.2022

BRIDON · BEKAERT
THE ROPES GROUP

Deep Wind Offshore Wind Cluster

- **Bridon-Bekaert**
- **Synthetic Mooring lines in shallow waters**
- **Rope solutions**
- **Scaling production capacity for Scotwind**
- **Scaling workforce**
- **Supply chain challenges**
- **Logistic challenges**
- **Commitment from Developers & Key stakeholders**
- **Partnerships & Strategic Alliances**

Mooring Subgroup 23. August 2022



BEKAERT AT A GLANCE

Preferred partner serving customers in 130 countries

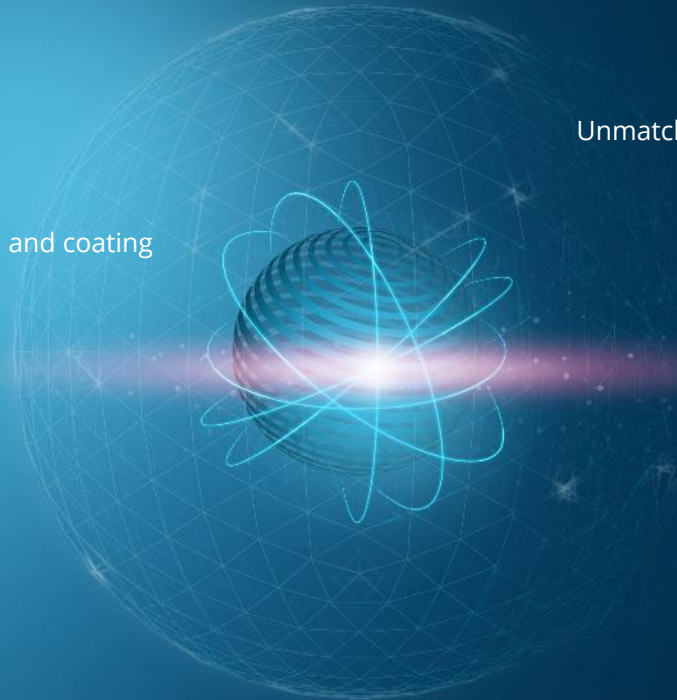
Global leader in steel wire transformation and coating technologies

Global manufacturing platform

More than 27 000 engaged employees worldwide

Corporate socially responsible company

Combined sales of € 5.9 b



WHAT SETS US APART

Unmatched products and solutions for customers across a wide range of industries

High-tech solutions leader with 1900 patents and patent rights in portfolio

Most advanced manufacturing capabilities

Experienced team with deep understanding of local customer needs

Ambitions and actions for a sustainable business

Creating value for our investors

Leading Through Innovation



BRIDON · BEKAERT
THE ROPES GROUP

Experience in Oil & Gas



- Supplied mooring lines to the first floating platform in 1983, Exxon Lena (Gulf of Mexico)
- Supplied mooring lines to first floating FLNG facility in 2013, Shell Prelude (Australia)
- Supplied first synthetic moored spar in 2004, BP Mad Dog Field (Gulf of Mexico)

Collaboration in Floating Offshore Wind



- Erocean
- Japan's 1st nylon mooring
- Mooring sense
- Ideol
- X1Wind
- Tampen
- Honey mooring
- Provence grand large
- Firm JIP Equinor
- Umain Aquaventus
- Gazelle
- Infloat

Mooring Line Considerations



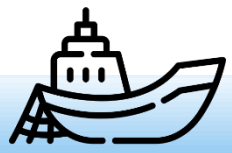
Seabed Contact



- ❖ Accelerated wear on jacket & traditional coating via abrasion
- ❖ Particle ingress leading to potential sub-rope damage



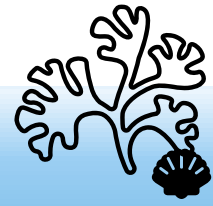
Mechanical Damage



- ❖ Represents 100% of observed failures for polyester ropes (May 22)
- ❖ Threats from impact events such as over-trawling



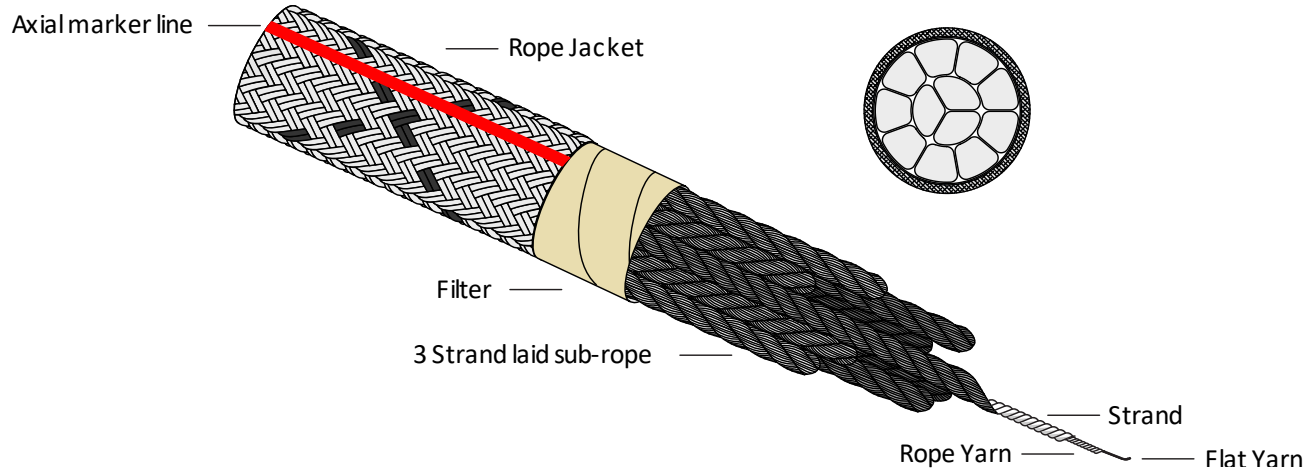
Marine Fouling



- ❖ Localised issue that usually occurs within top 30m of water
- ❖ Additional weight and potential penetration / damage



- Bridon Synthetics MoorLine rope consists of:
 - Core of multiple, parallel laid sub-ropes
 - Polyester, Nylon or HMPE fibres
 - Braided jacket
 - High performance fabric filter
 - Binds structure of the rope together and protects the core and filter



“MoorLine” by Bridon-Bekaert

A Rope Specifically Developed for Offshore Mooring



BRIDON · BEKAERT
THE ROPES GROUP



Sub-Rope

- 3-strand parallel laid sub rope, 12-strand available for TLP applications
- Low-twist ropes that retain 70-72% of yarn strength, conventional laid construction retains 45-60%



Filter System

- High performance fabric filter
- Protection from particles down to 5 microns

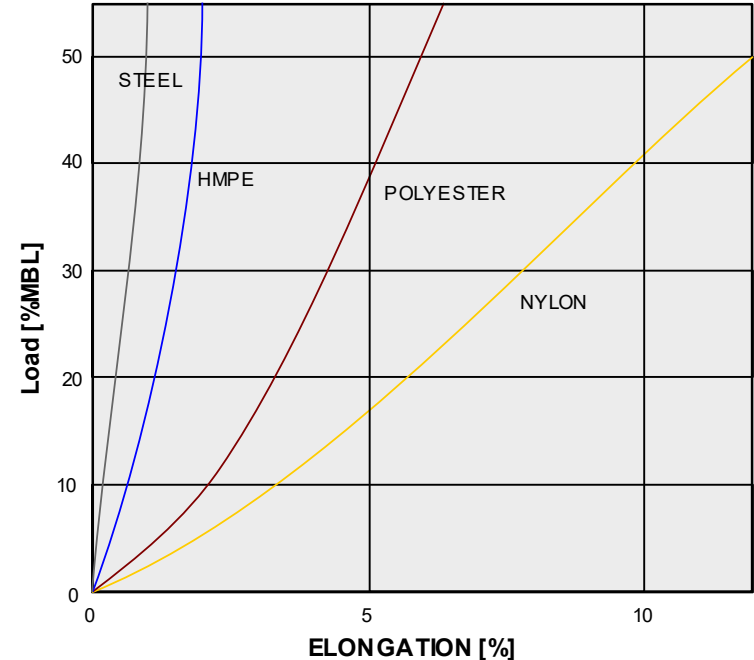


Braided Jacket

- Braided jacket binds structure of the rope while protecting the sub-ropes and filter
- Axial marker line and twist marker allows identification of twists within rope



- High tenacity Polyester
 - 20+ years of proven performance and reliability
 - Mid range stiffness characteristics
- Low creep HMPE:
 - Suitable for TLP moorings due to its high tensile strength and high stiffness
 - Lifetime can be engineered for 25 years, in accordance to predicted load scenario
 - Lower weight and easier installation when compared to steel
- High tenacity Coated Nylon
 - Next slide



MoorLine | It takes the 'Right Materials'



BRIDON · BEKAERT
THE ROPES GROUP

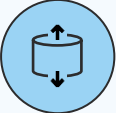
Polyester

Nylon

HMPE



Strength



Modulus

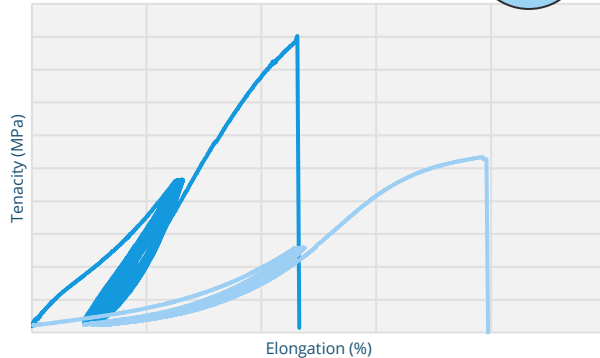


Cost





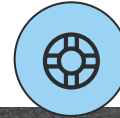
Nylon Qualification



- Greater elongation compared to polyester
- Similar compliance with shorter lines*
- Ideal for shallow water sites (<100m) with harsh waves (>5m)
- DNV qualification underway

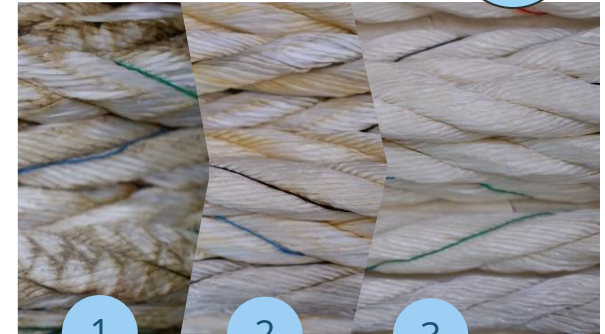
*when compared to polyester

Integrated Buoyancy



- Rigid high density foam to maximise floatability & certified for sub-surface use
- Compact design fully integrated into rope & can be distributed in specific locations
- Reduces mooring line components
- Still possible to bend/spool rope

Advanced Coating



- **1. Braided Jacket:** Intrusion, staining, no significant damage to sub-rope
- **2. Jacket + Filter:** No intrusion, staining, no damage to sub-rope
- **3. Jacket + Filter + Coating:** No intrusion, no staining, sub-rope "like new"

- Sub-rope condition after strip down

Braided Jacket



- Particulate and shellfish intrusion
- Staining
- No significant damage to core

Braided Jacket +
5-micron particle filter



- Staining
- No particle ingress detected

PU overlay Braided Jacket +
5-micron particle filter



- No staining
- No particle ingress
- "like new" sub-ropes

Advanced Composite Structure

An enhanced protection layer has been developed, that combines the know characteristics of the Polyester Braided Jacket with a polymeric matrix. This creates a composite structure that addresses the main failure mechanisms that were identified from seabed contact field trials:

- High abrasion resistance
- High tear resistance
- High elongation (low/no effect axial stiffness)
- Chemically inert
- Long lifetime

Cutting protection is also based on the same platform

- Composite structure enables adding different levels of cut protection

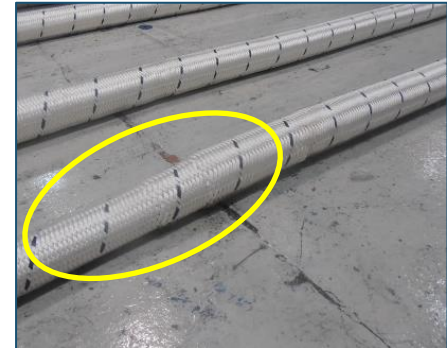
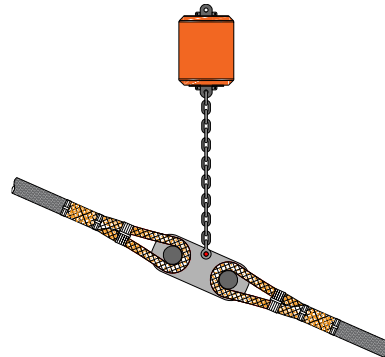
Testing of Jacket composite structure

- Lab tests and field trials made to confirm the suitability of the protection layer.
- Seabed drag testing conducted vs. base case Moorline rope.
 - Specimens were repeatedly dragged, lifted/dropped, and abandoned
 - Damage due to abrasion and particle ingress of each rope was documented..

Currently under discussion with class societies and lead users



- Why is buoyancy needed:
 - Keep rope off sea bed (e.g. Fouling weight, Leeward lines)
 - Modify mooring response
 - Inverse catenary
- Effective, economical solution developed compatible with all other line features
 - Fully integrated (protected), flexible and scalable
 - Drastic reduction in component count.



Industrial grade rope terminations



- Human-factor
- Labor and time intensive
- Splice setting variation



- Industrial process

- Higher output
- Easier to scale (Industry 4.0)
- Subrope condition monitoring functionality
- Reducing human factor variation
- Suitable hardware substrate for **monitoring**

100% Strength efficiency

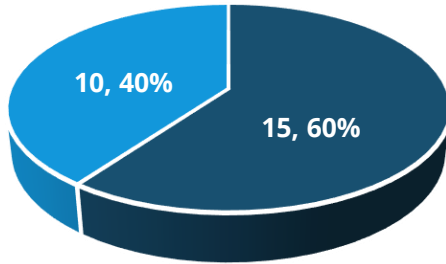
100% length accurate

100% repeatable



Market Requirements & Dependencies

ScotWind: 25GW Offshore Wind



• Floating • Fixed

- Assuming 15MW turbines: 15GW floating equates to 1,000 floaters
- Each floater requires 4-6 mooring lines therefore 4,000-6,000 lines over the next 10 years



Production



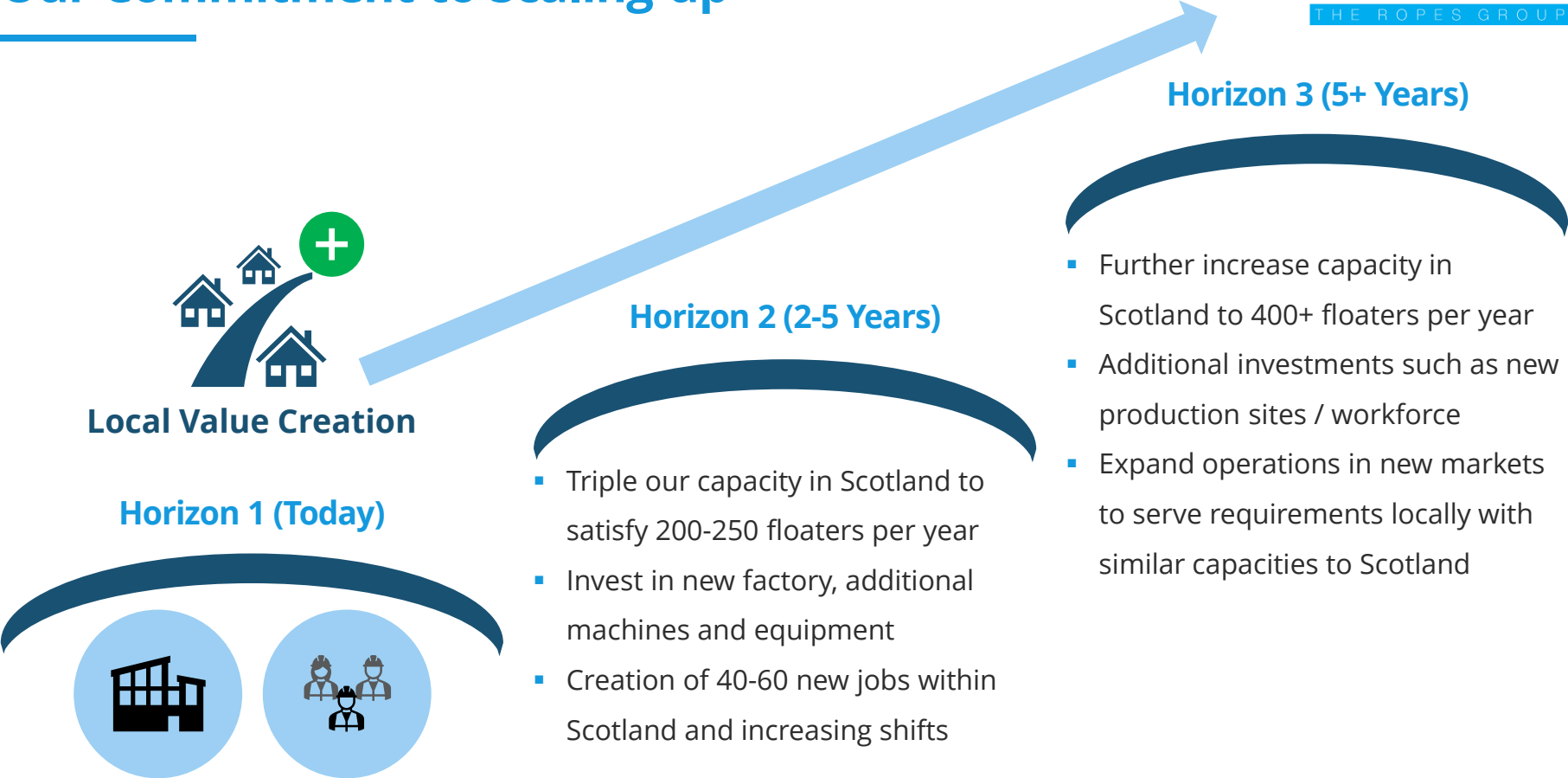
- Current capacity at BBRG is 200-300 mooring lines per annum
- Therefore can satisfy the needs of 30-75 floaters per annum
- 15-30 years to meet requirement of ScotWind alone

Workforce



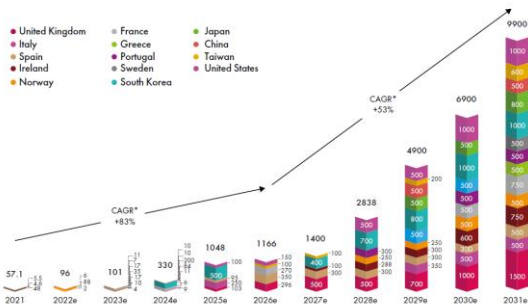
- Current workforce employed in Scotland is approx. 40 people
- Operators, Innovation Engineers Project Teams
- Based in Coatbridge with no dedicated resource in Grangemouth

Our Commitment to Scaling-up



Infrastructure and supply chains need to be ready in advance of the industry scaling up

New floating wind installations, Global (MW)**



**Composed Annual Growth Rate. **Note: the floating wind output is already included in ORECA's global offshore wind forecast. Source: ORECA's market intelligence team, June 2022

Combined with training to ensure people have the skills required in advance



Supply Chain



Infrastructure

- Reels for mooring lines are made to measure, standardisation would result in supply chain efficiency as reels could be reused
- Typically fewer/large reels are used to reduce cost however more/small reels offer logistical benefits via shipping containers
- Scaling of mooring line capacity is relatively easy when compared to heavier mooring components such as anchors, chains and floating foundations as they are typically setup for oil and gas
- Ports will need investment for floating foundation construction, mooring systems as well as storage facilities
- Access will be required to cranes for heavy lifting, which could also lead to investment in strengthening port foundations
- Vessels could become a bottleneck, potential to utilise alternative vessels or depending on reels dimensions and reel solution, container vessels.
- Predictable Freight cost internally between loading port and fabrication site

How will this be possible?

